

**INDUSTRIAL STEAM GENERATION
BY NON-IMAGING FOCUSING**

FINAL REPORT

FEBRUARY, 1979

PREPARED BY:

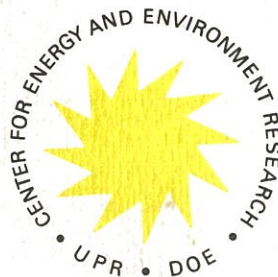
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UNIVERSITY OF PUERTO RICO — U.S. DEPARTMENT OF ENERGY

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1. Introduction

An innovative solar collector for industrial steam generation has been designed, developed and built by CEER with cooperation and funding from the University of Chicago and Bacardí Corporation. The collector is a linearly segmented compound parabolic concentrator (CPC) with a cylindrical evacuated tube as the receiver. As part of the project, a solar radiation measuring station was installed on the premises of the Bacardí Rum Distillation Plant in Cataño, Puerto Rico.

This report emphasizes that portion of the project carried out after the First Progress Report of August, 1978. We refer the reader to that report for details of the initial phases of the project. In general, that report dealt with the general design ideas and the preliminary analytical studies of these ideas. Some work with an experimental model was also included. This report covers mainly the final design and construction of the collector.

The main design elements that are incorporated in this collector are now summarized. First, it is a CPC collector with a concentration ratio of 5.25. This means it can make use of diffuse as well as direct sunlight. This also means it does not require continuous or even daily tracking of the sun's position. Second, it has an evacuated tubular receiver of a new design. This receiver is expected to perform better than other receivers for high temperature collectors. Third, the CPC mirror surface is segmented and encapsulated in glass tubes. The tubes provide

lightweight, low cost structural support as well as protection for the mirror surface.

II. Design and Fabrication of Collector Components

The major system components of the linearly segmented compound parabolic collector under consideration are shown in schematic form in Figs. 1, 2, and 3 which show the evacuated tubular receiver, the segmented encapsulated mirrors and the collector frame. Dimensions given in these drawings were original design and some were changed in the final design.

A. Evacuated Tubular Receiver

Fig. 4 shows the schematic of the single wall evacuated receiver tube designed specifically for this project. A detailed description of this receiver was given in the First Progress Report.

One of the three receiver tubes received from the manufacturer was tested under stagnation conditions and one sun radiation density. The temperature inside the copper tubing was found to be 240°C attesting to the excellent heat absorption and retention qualities of this receiver design.

B. Segmented Mirror

A major part of our effort since August has gone into developing and building the segmented mirror. Figure 5 illustrates the final design of the mirror units.

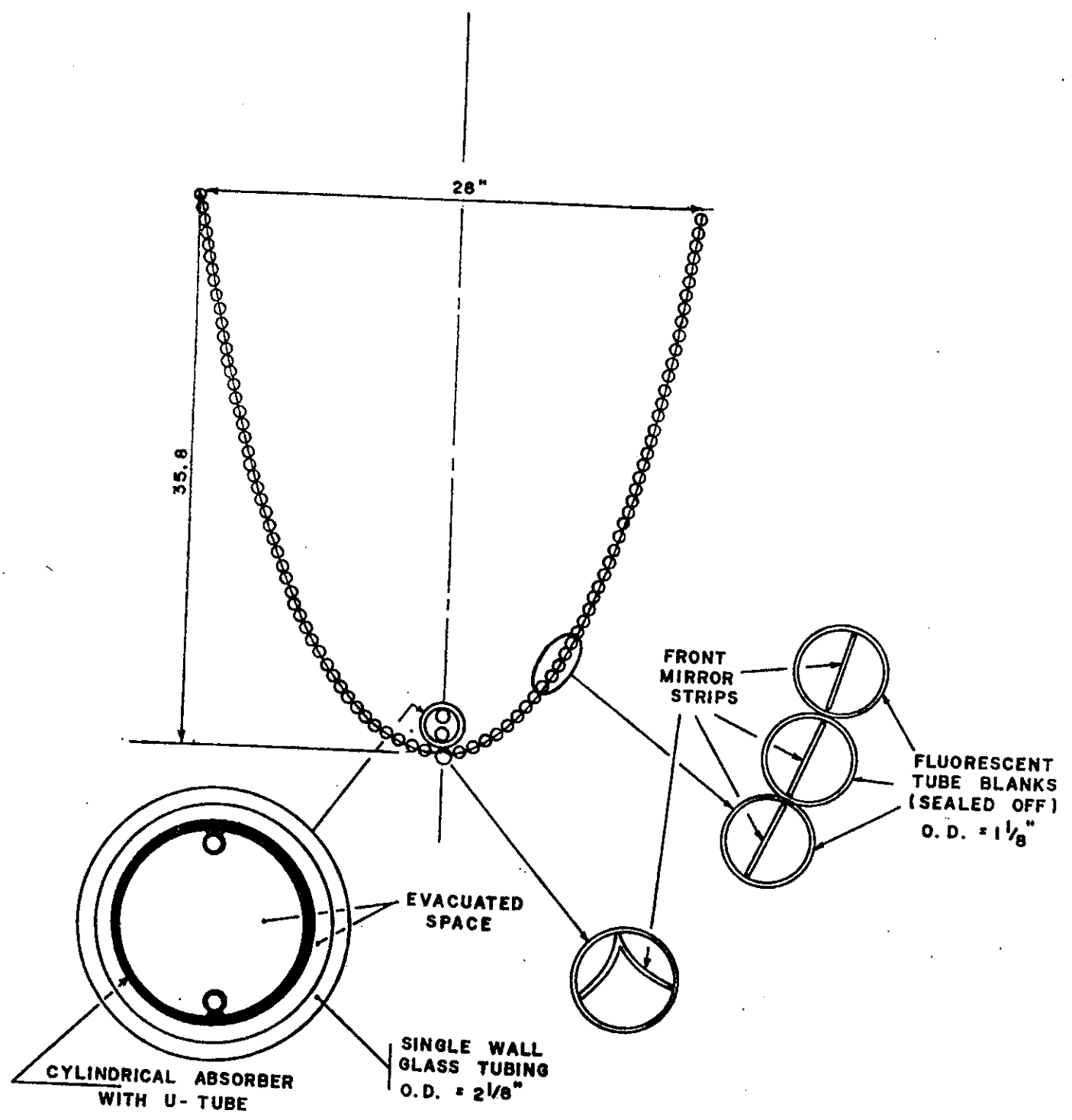
Plexiglas plastic (1/8" thick) was chosen as the material for the mirror substrate. Major considerations in this decision were ease of handling, cutting, and machining, and

FIGURE -1-

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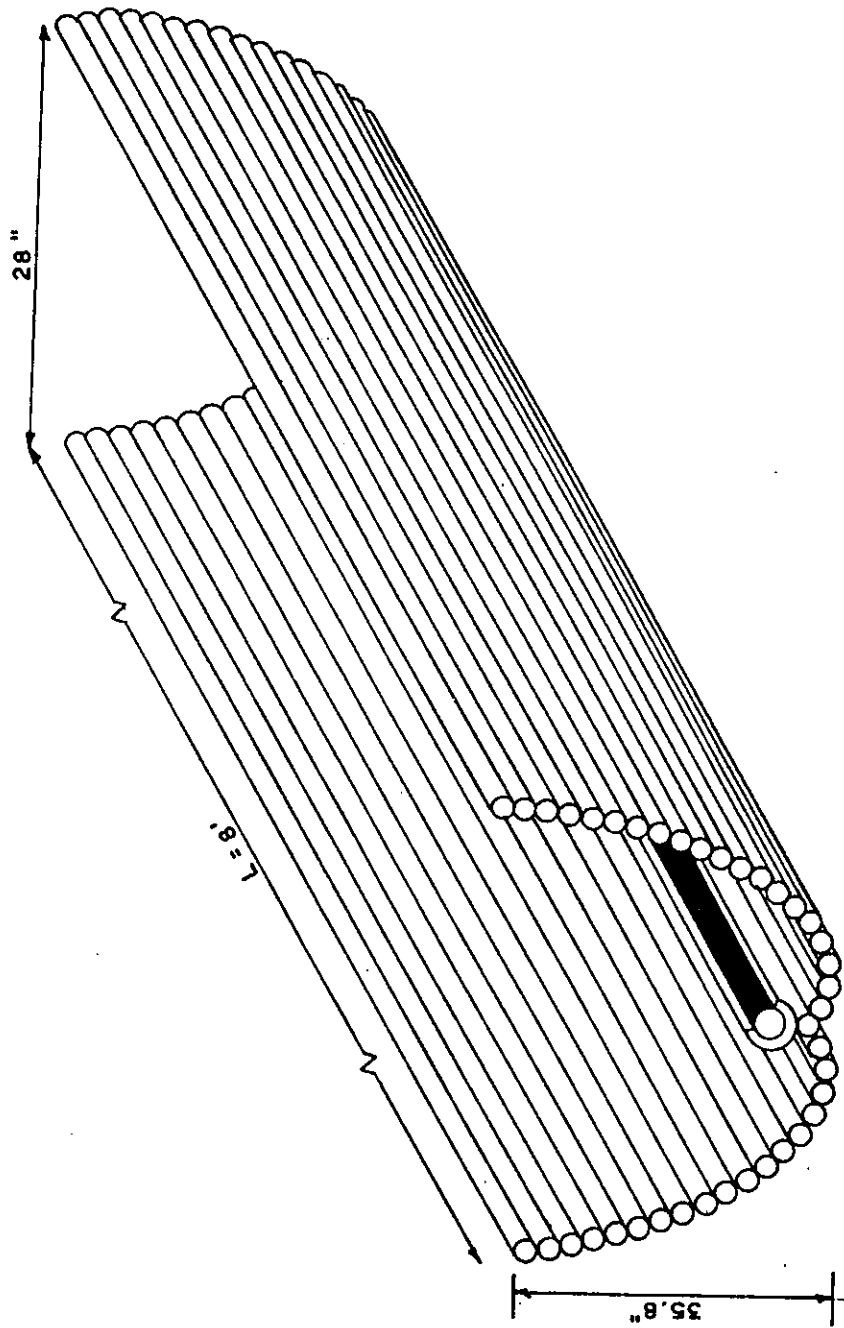
FACETED CPC COLLECTOR (EFF. CR \approx 5)

(SUPPORT FRAME FOR TUBES NOT SHOWN)



DRAWING NOT TO SCALE

FIGURE -2-
PHYSICAL DIMENSIONS OF THE PROTOTYPE CONCENTRATOR SYSTEM



NOT TO SCALE

FIGURE -3-
DUAL AXIS COLLECTOR FRAME

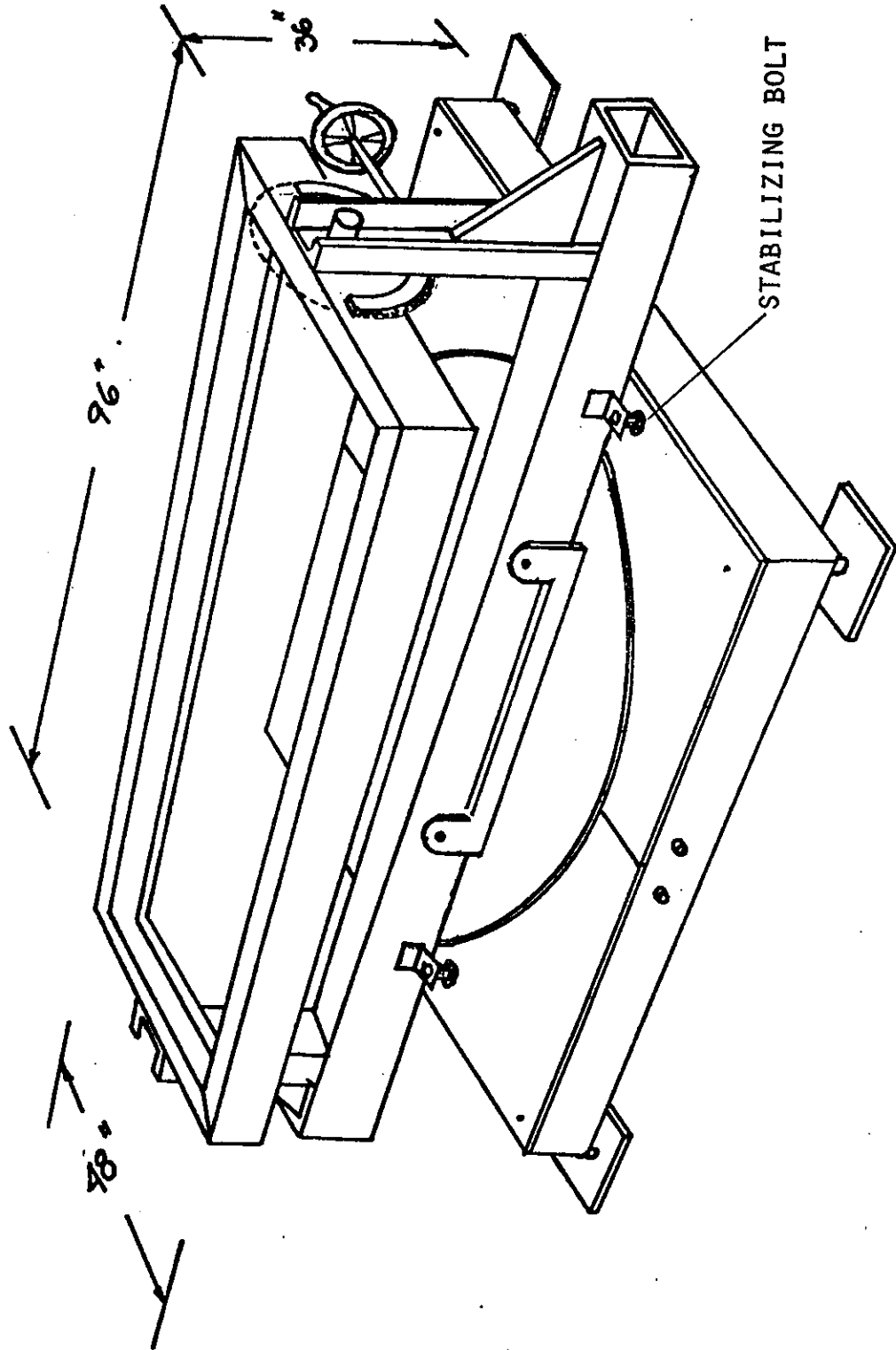


FIGURE -4-

EVACUATED RECEIVER TUBE TO BE UTILIZED WITH THE LINEAR SEGMENTED
COMPOUND PARABOLIC CONCENTRATOR

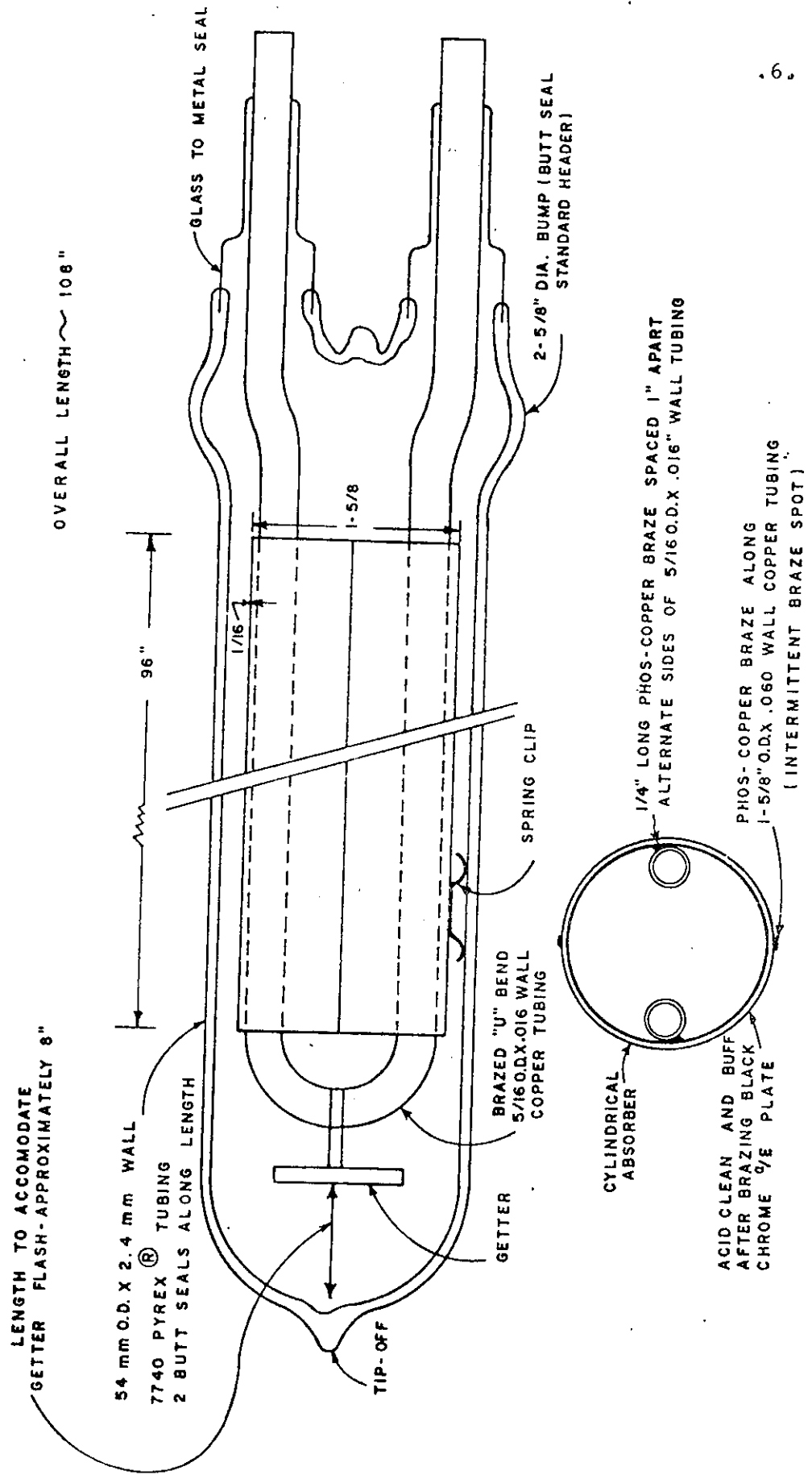
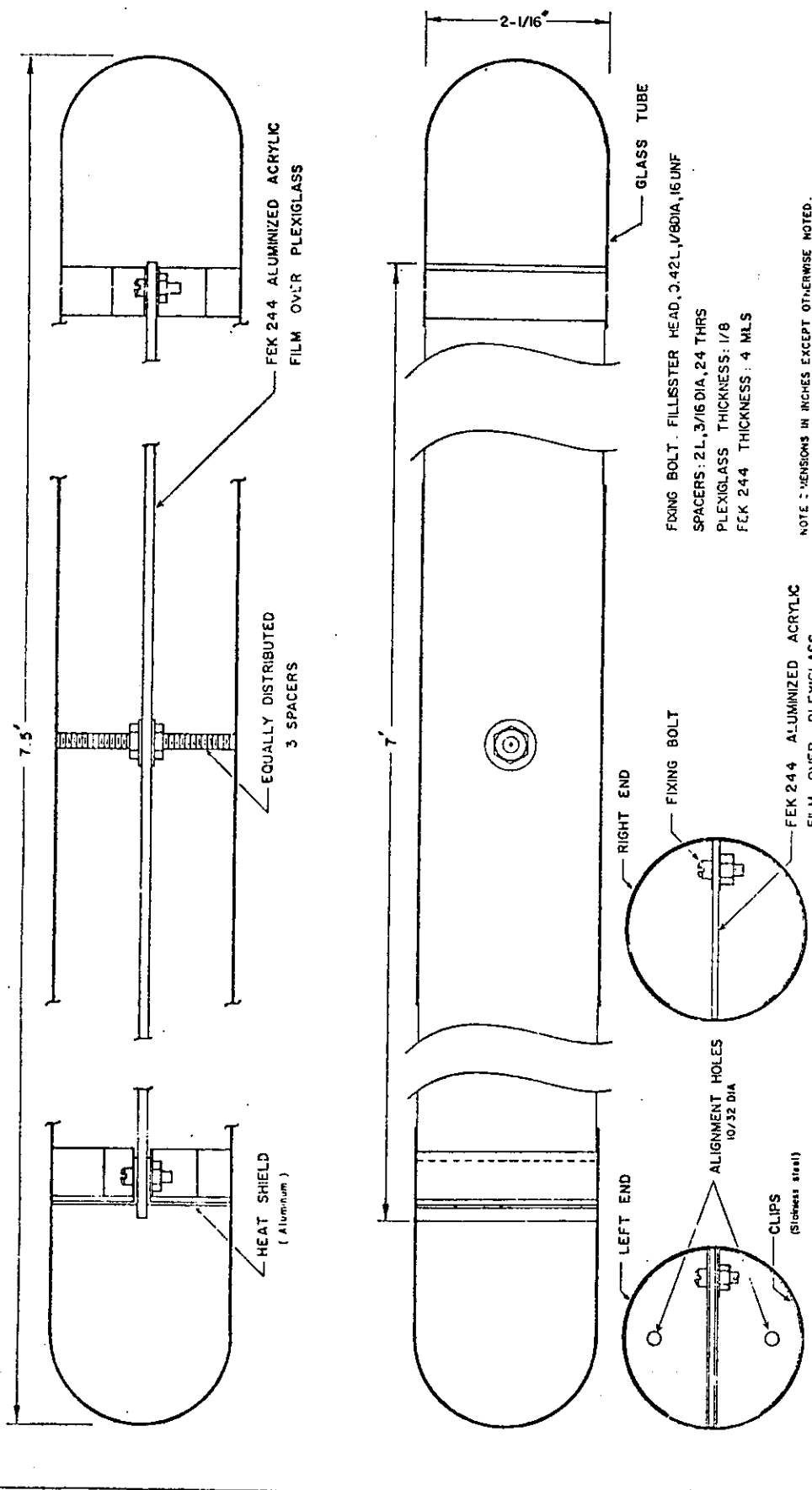


FIGURE -5-



MATERIAL: As shown above		DESCRIPTION: ENCAPSULATED MIRROR SEGMENT		DWG NO:	
PART NO: —		SCALE: 2 1/2"		CEER — CENTER FOR	
PCS/UNIT: 38		DATE: February 1979		ENERGY AND ENVIRONMENT RESEARCH	
		DR: J. F. Gumarro			
		CK: —			
		TCR: —			
		APP: —			

smoothness of surface. The plexiglas was cut into strips 7' long and 1 15/16" wide.

Finding a suitable reflective film and a method of bonding to the plexiglas was a major problem. Much effort was spent in trying to bond 200 Dun-Chrome[®], DL-50 metallized polyester film (Dunmore Corp., Newtown, Penn.) to the plexiglas with unsatisfactory results. Many different types of bonding agents were tried. Finally we learned of a new product manufactured by the 3M Company. This is their "Scotchcal" Brand Film FEK-244, a 0.004" thick aluminum-on-acrylic film with 86% spectral reflectance. This film has pressure-sensitive adhesive backing and satisfactory results were obtained in applying it to the plexiglas substrate.

The encapsulation tubes are fluorescent tube blanks obtained from Corning Glass Works (Fig. 6). These have an outside diameter of 2.08" and a wall thickness of 0.035". We estimate the diameter tolerance to be ± 0.01 ".

The mirror segments are held inside the glass tubes by spring clips at the ends. In order to prevent undue sagging of the mirror, it was found necessary to attach three screw spacers at equal intervals along its length. A metal heat shield was also attached to prevent damage to the mirror when the glass tube was being closed off.

After attaching clips, spacers and shields to the mirror, the assembly was inserted inside a glass tube (Fig. 7). The mirror was then checked to determine whether there was any twist

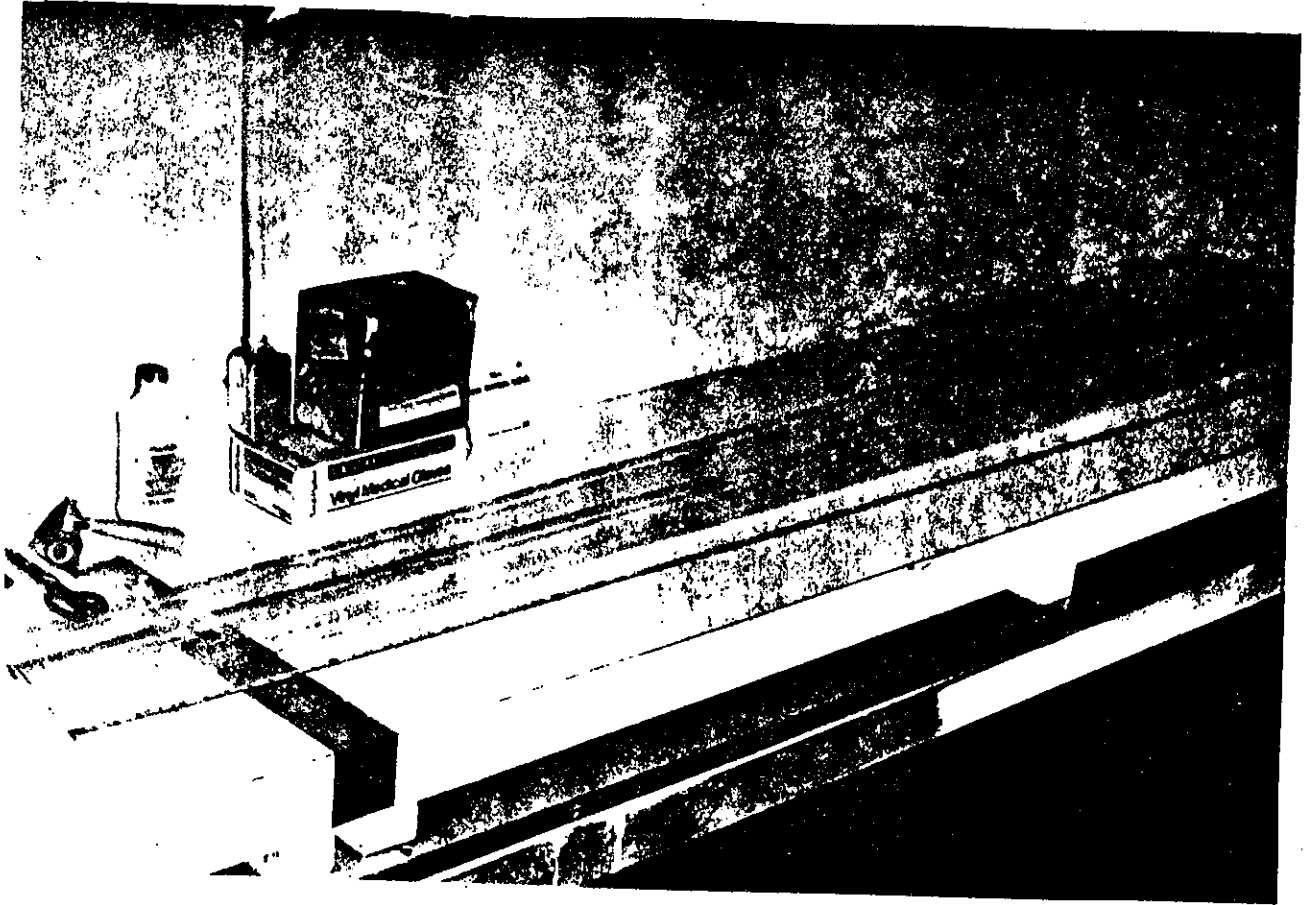


FIG. 6 FLUORESCENT TUBE BLANKS FROM
CORNING GLASS WORKS.

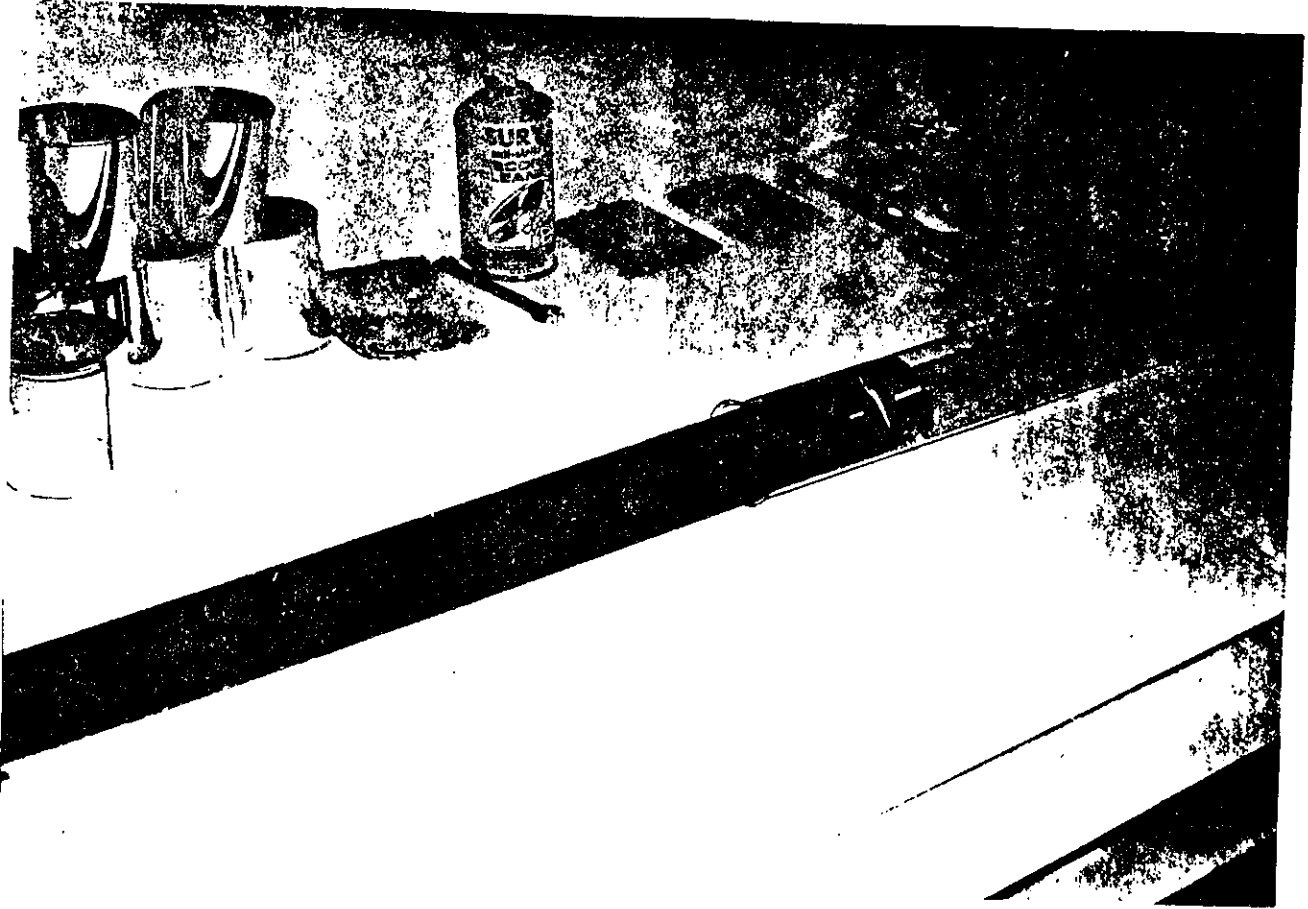


FIG. 7 INSERTION OF MIRROR ASSEMBLY INTO GLASS TUBE.

of one end with respect to the other. This was done by looking at the reflection of a laser beam from the mirror at different points along its length (Fig. 8). Since one end of the mirror was accessible and since the spacers were not attached to the tubes, any large twists could be removed. The largest allowable amount of twist of one part of the mirror with respect to another was 1° .

Originally it had been planned to close off the glass tubes after they had been evacuated at an elevated temperature and filled with a dry gas. The idea was to eliminate as much moisture as possible from the inside of the tubes. An oven was built and it was determined that the mirrors could withstand 100°C without apparent damage. However, when the tubes were evacuated to a pressure of 500 microns of Hg. at 100°C , immediate damage to the adhesive bond resulted. Evacuation alone did not appear to damage the bond and several tubes were made using this procedure. After being connected to a vacuum pump for 30 minutes, they were filled with dry nitrogen at a pressure of ~ 1 atm.. Damage to the adhesive bond of these mirrors did not become apparent until they had been exposed to sunlight for 2 or 3 weeks. Finally it was decided to abandon the evacuation procedure. Tubes were closed off in an air conditioned room. A room dehumidifier brought the relative humidity down to 50% at 75°C which corresponds to a ratio of moisture to dry air of 1.0% by weight.

Another important problem encountered in the construction of the tubes was the frequent breakage and cracking

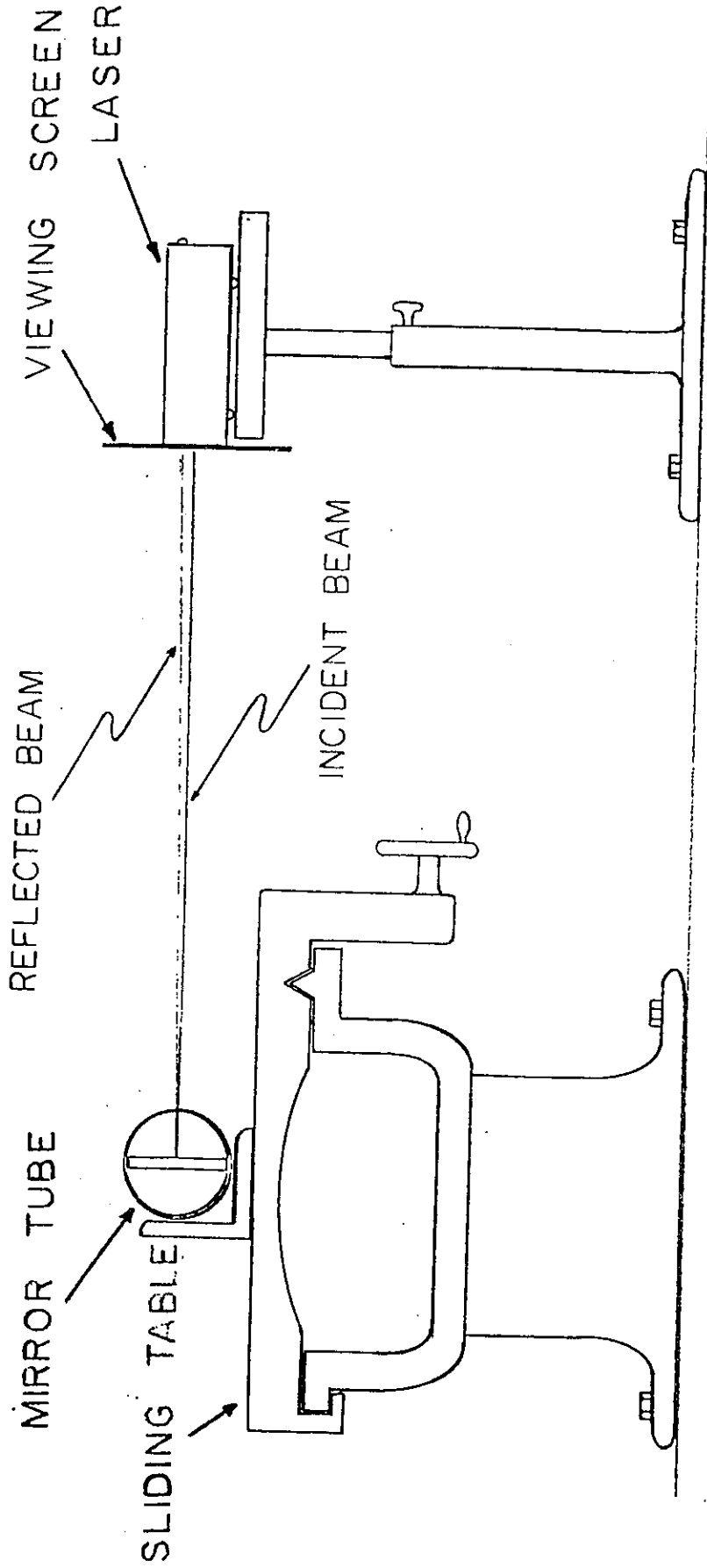


FIG. 8 SCHEMATIC OF THE METHOD FOR MEASURING TWISTS IN MIRROR SURFACE. THE SLIDING TABLE MOVES THE MIRROR TUBE ALONG ITS LENGTH (I.E. PERPENDICULAR TO THE VIEW SHOWN). ANY CHANGE IN THE POSITION OF THE REFLECTED BEAM AS THE SLIDING TABLE MOVES IS AN INDICATION OF TWIST.

of the glass at stress points where it had been worked. Since the temperature of the mirrors could not be raised, it was not possible to do oven annealing to relieve these stresses. This problem was alleviated considerably when the evacuation procedure was abandoned. It seems that a large part of the problem was due to differences between the nitrogen pressure inside and atmospheric pressure outside. This resulted in uneven tips which eventually cracked.

C. Collector Frame

Figs 3 and 9 show the collector frame including the tube wells which actually hold the glass tubes.

The basic dual axis tracking frame design developed by the University of Chicago was altered in some important ways. The main beam of the frame which in the Chicago design was an I-beam was found to be too unstable to torsional forces such as would be exerted on it by the collector weight when tilted. The I-beam was replaced by a rectangular cross section hollow beam which also allowed a simpler design for fixing the beam to the circular platform.

Four bolts were added to the sides of the main beam. These prevent movement of the circular platform (and thus of the collector) after it has been set at a particular position.

In order to measure the collector's tilt angle, two bubble level with protactor assemblies were installed at each end of the collector frame. These permit angle measurements with an accuracy of $\sim 1/4^\circ$.

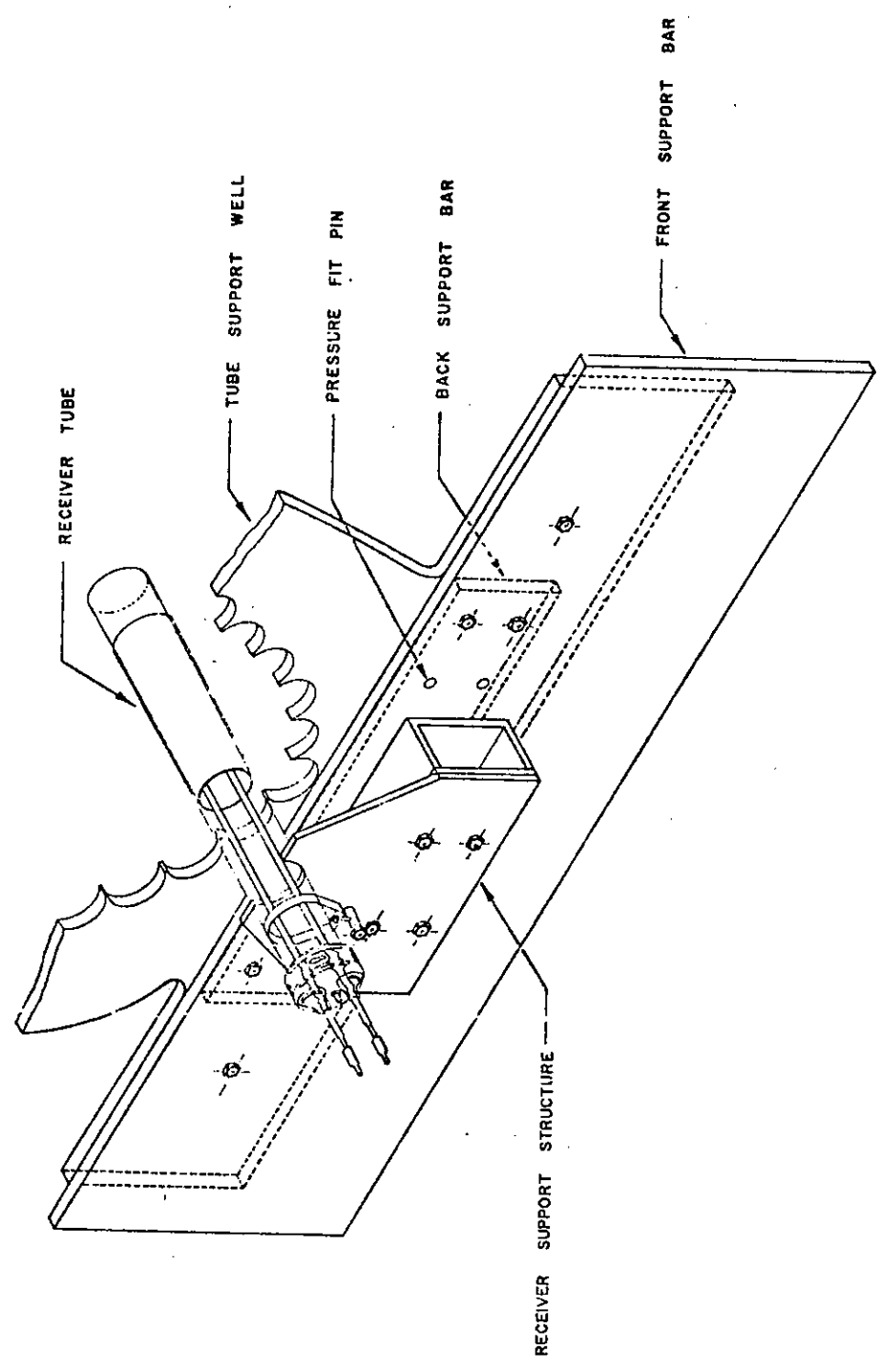
Major efforts on the collector frame went into designing and building the tube wells which are shown in detail in Fig. 9.

A computer program was developed to calculate the theoretical shape of the reflector surface (See First Progress Report, Appendix A). Using the results from the program, the tube wells were precisely machined. Four identical pieces (each was one-half a well) were machined simultaneously by stacking them. The raw material for the wells were four pieces of 1/2" aluminum, 20" wide and 48" long. The circular holes that hold the tubes have a diameter of 2.09". The straight line distance between circles is 2.11" to allow for the metal bands that grip the tubes. After the tube holes had been machined, excess material was removed to make the structure lighter. The tube holes thus became open semicircles.

Fig. 10 is a depiction of the support bar and the structure which holds the receiver tube. These can also be seen in Fig. 9. Two halves of a well were held together by precisely machined pressure fit pins and by screws and nuts which joined them to the support bar. The pressure fit pins assured alignment to a high degree of precision. The receiver tube is supported by a structure that allows space for the mirror tubes that are close to the receiver.

The mirror tube wells are fastened to cross support members of the frame. Six aluminum tubes join the tube wells to each other. These add much rigidity to the structure

FIGURE -10-



MATERIAL: As shown above		DR: J. F. Gomara		SCALE: 1" = 2"		DWG NO:	
PART NO: ---		CK: ---		DATE: February 1979		CENTER FOR ENERGY AND ENVIRONMENT RESEARCH	
PCS / UNIT : ---		TCR: ---		APP: ---			

and very little weight.

The structure for fastening the glass tubes to the wells is shown in Fig. 11. It consists of a stainless steel band which is pulled tight by a screw which runs through a bolt fastened to the frame. The bands are placed so that bands from neighboring tubes do not touch thus reducing the distance between mirror segments.

III. Analytical Studies of Collector Orientation

One of the main advantages of a CPC design is the possibility of doing away with continuous tracking of the sun thus reducing complexity and cost. This is because a CPC can collect radiation incident over an extended range of angles as is shown in Fig. 12. Our CPC design is an ideal 6.30 X concentrator truncated to 5.25X. The theoretical half acceptance angle (θ_c) of the ideal concentrator is 9° . An actual device never has a perfect theoretical shape due to random deviations of its surface from the "ideal" surface. This changes its acceptance characteristics (see Fig. 12) but this change can be approximated as a reduction in the acceptance angle.

The idea, then, is to orient the collector so that the radiation is incident at an angle less than or equal to the acceptance angle. Yet we want to do this with a minimum amount of tracking. The optimum collection to tracking ratio is achieved by orienting the long axis of the collector along the east-west direction. The angle of interest is then the projected incidence angle on the plane defined by the zenith and the

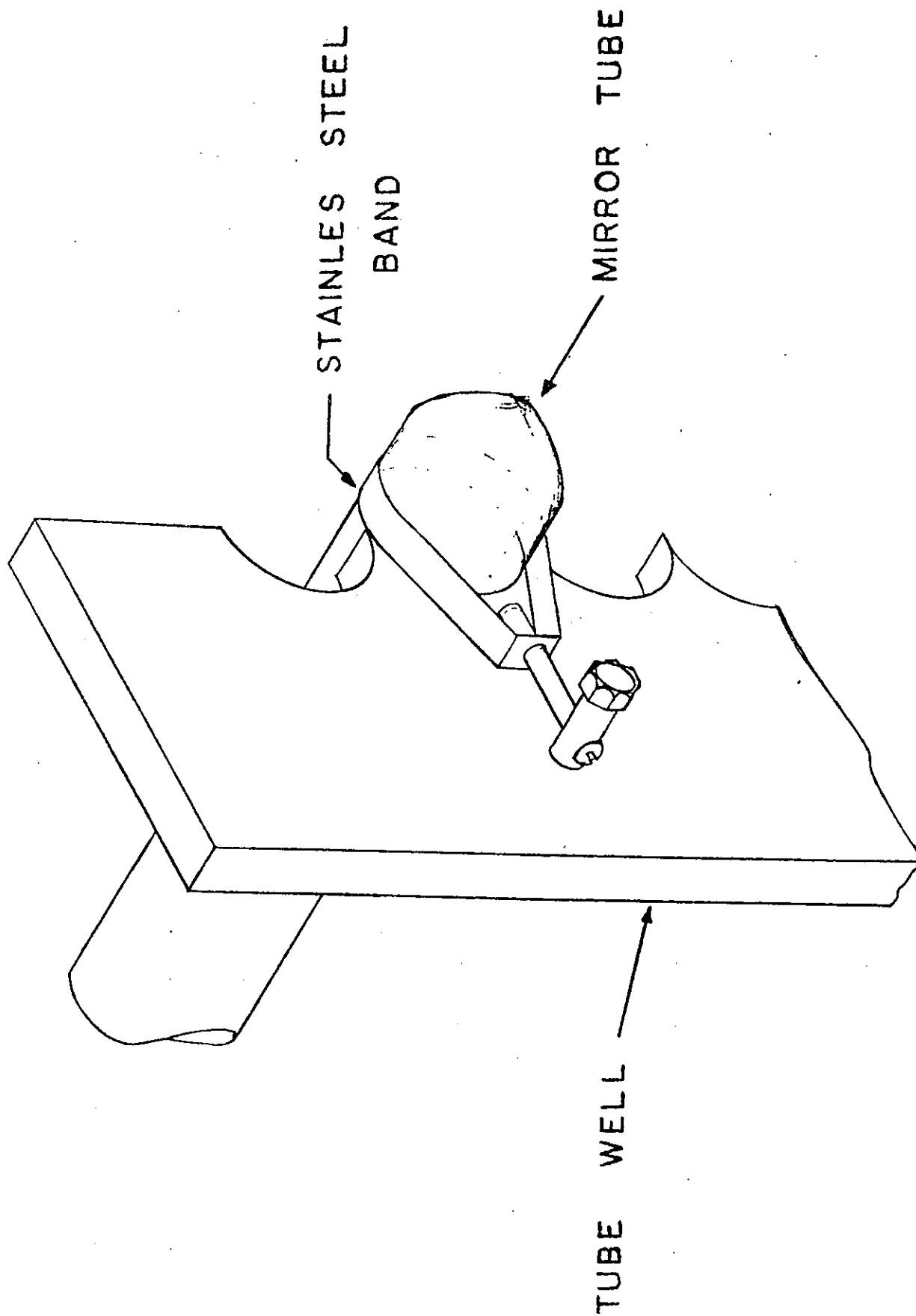


FIG. 11 ATTACHMENT OF MIRROR TUBES TO TUBE WELL.

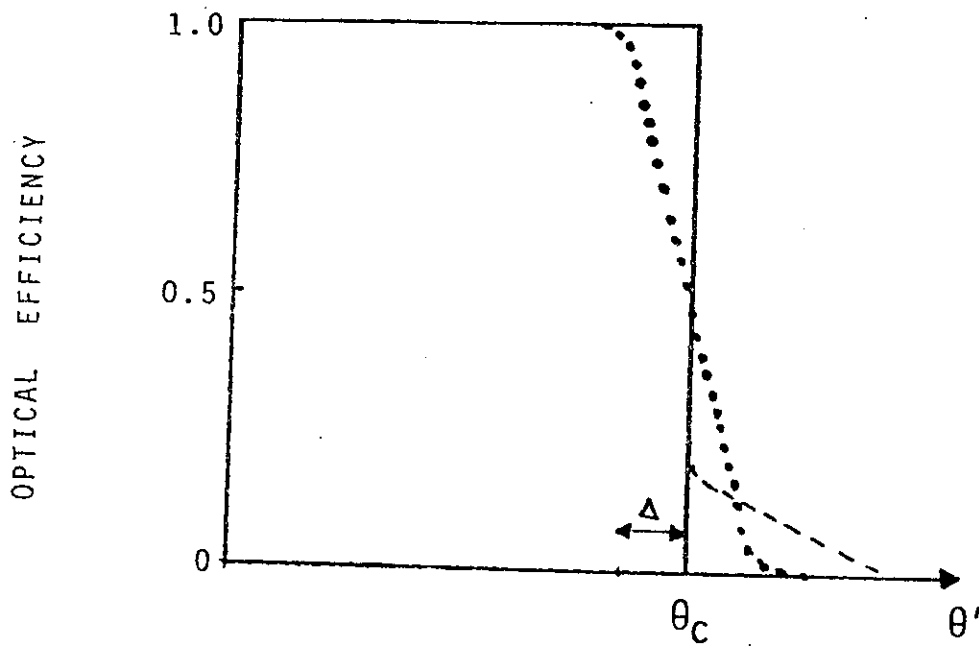


Fig. 12 Fraction of the radiation incident on the aperture of a CPC at angle θ' which reaches absorber. All curves refer to a concentrator in two dimensions with acceptance half angle θ_c , assuming perfect reflectivity.

- untruncated ideal concentrator
- - - - - truncated ideal concentrator
- untruncated concentrator with average surface error Δ .

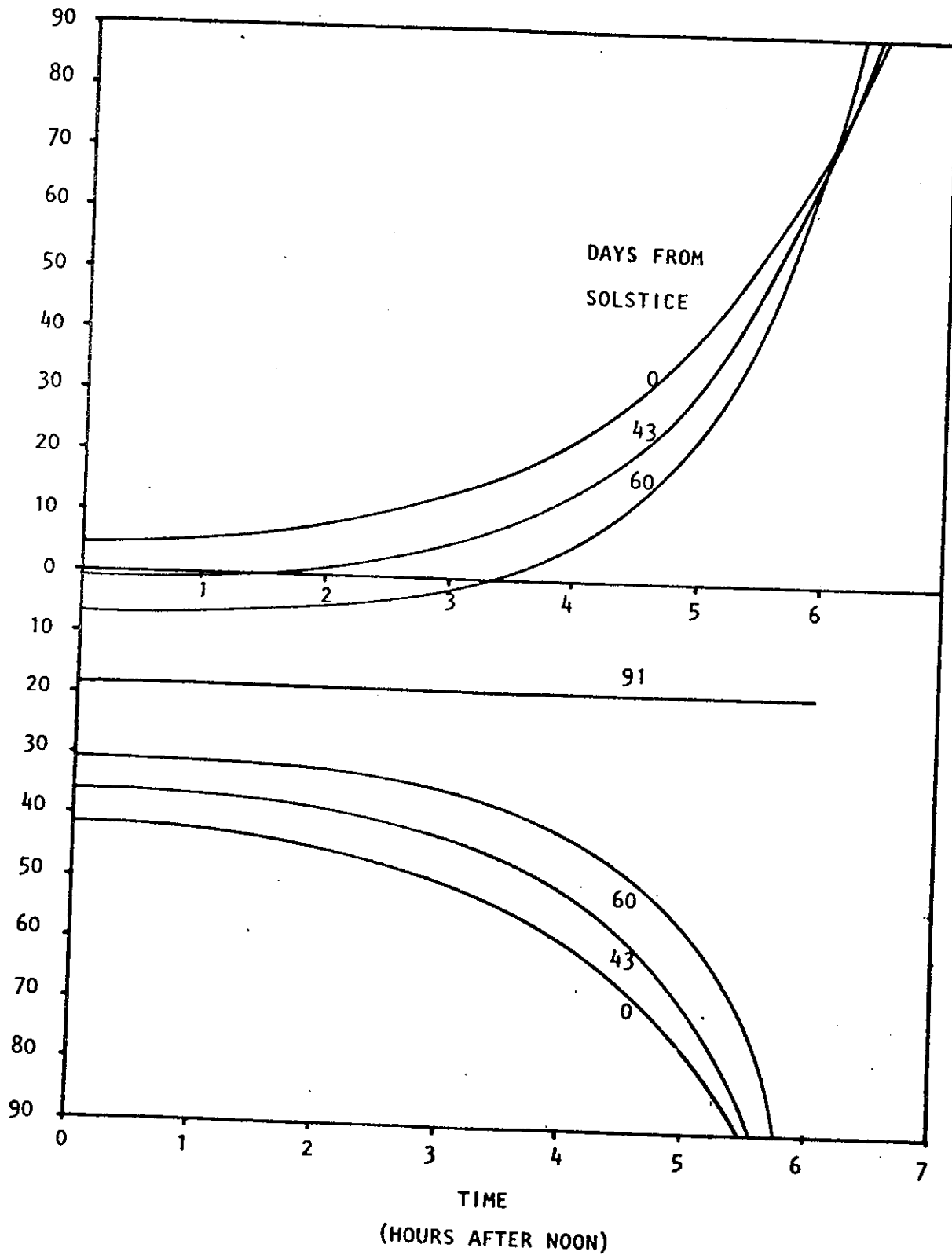
north-south direction. This angle (θ_{sp} , measured from the zenith) can be calculated for a particular day and hour by the following formula

$$\tan (\theta_{sp} + \alpha) = \tan \delta / \cos \omega$$

where α is the latitude, δ is the declination and ω is the angular time from noon ($\omega = 2\pi t/24$, t in hours). Fig. 13 is the graph of θ_{sp} for different days during the year and for Puerto Rico's latitude.

A scheme for orienting the collector can be derived from this graph. One first chooses a half acceptance angle (θ_c) and a minimum daily collection time (e.g. 7 hours/day). Starting at the summer solstice, one determines the value of θ_{sp} at the extremes of the minimum collection time (time=3.5). Call this angle θ_e . Before and after the solstice the collector would be oriented at an angle $\theta_e - \theta_c$. For this configuration, the collector would have a high optical efficiency at any hour of the day that $\theta_e - 2\theta_c < \theta_{sp} < \theta_e$. For several days after the solstice this condition will hold more than 7 hours a day. But there comes a day when it will hold for less than the required 7 hours because it will not hold in the period around noon time. On this day, the collector orientation should be changed. Suppose that the value of θ_{sp} at the extremes of the minimum collection time on this day is θ'_e . The collector is then pointed at an angle $\theta'_e - \theta_c$. This procedure for determining the collector orientation and the dates for changing it is repeated until a full year is mapped out. The result is a chart such as the one

FIG. 13
PROJECTED
SOLAR ELEVATION
(FOR LATITUDE 18.5)



shown in Table 1. For a half acceptance angle of 9° and a minimum required collection time of 7 hrs./day the collector has to be reoriented only 10 times a year.

IV. Insolation Measurements

Solar radiation has been recorded at the Bacardí plant in Cataño since July, 1978. Diffuse as well as total insolation have been recorded. Details of the measuring process were given in the First Progress Report.

Results of the computer analysis of data for the months of July, August and September are given in Appendix A. Data for the months of October, November and December shows certain irregularities which are not understood at present. These months are not included in the Appendix.

V. Conclusion

The completion of construction of an innovative experimental solar collector designed for industrial steam generation is the main achievement of our work this year. In addition, much analytical study of the design has been made and a solar radiation measuring program has been implemented at the proposed industrial site. The analytical studies indicate the possibility of a high efficiency to cost ratio for this collector. Figures 14, 15, 16 and 17 are views of the finished Bacardí solar collector.

TABLE 1

$\theta_C = 9^\circ$

*START DATE	*END DATE	TILT S=south N=north	LENGHT OF PERIOD	DECLINATION AT END OF PERIOD
Jan. 30	Feb. 24	37°S	25 days	-10°
Feb. 24	Mar. 22	25.0°S	26 days	0
Mar. 22	Apr. 17	11°S	26 days	10°
Apr. 17	May 12	1°S	25 days	18°
May 12	Jul. 31	11°N	80 days	18°
Jul. 31	Aug. 26	1°N	26 days	10°
Aug. 26	Sep. 20	11°S	25 days	0
Sep. 20	Oct. 16	25°S	26 days	-10°
Oct. 16	Nov. 11	37°S	26 days	-18°
Nov. 11	Jan. 30	45°S	80 days	-18°

No. of adjustments/year = 10

*In a leap year, add one day to dates after Feb. 28.

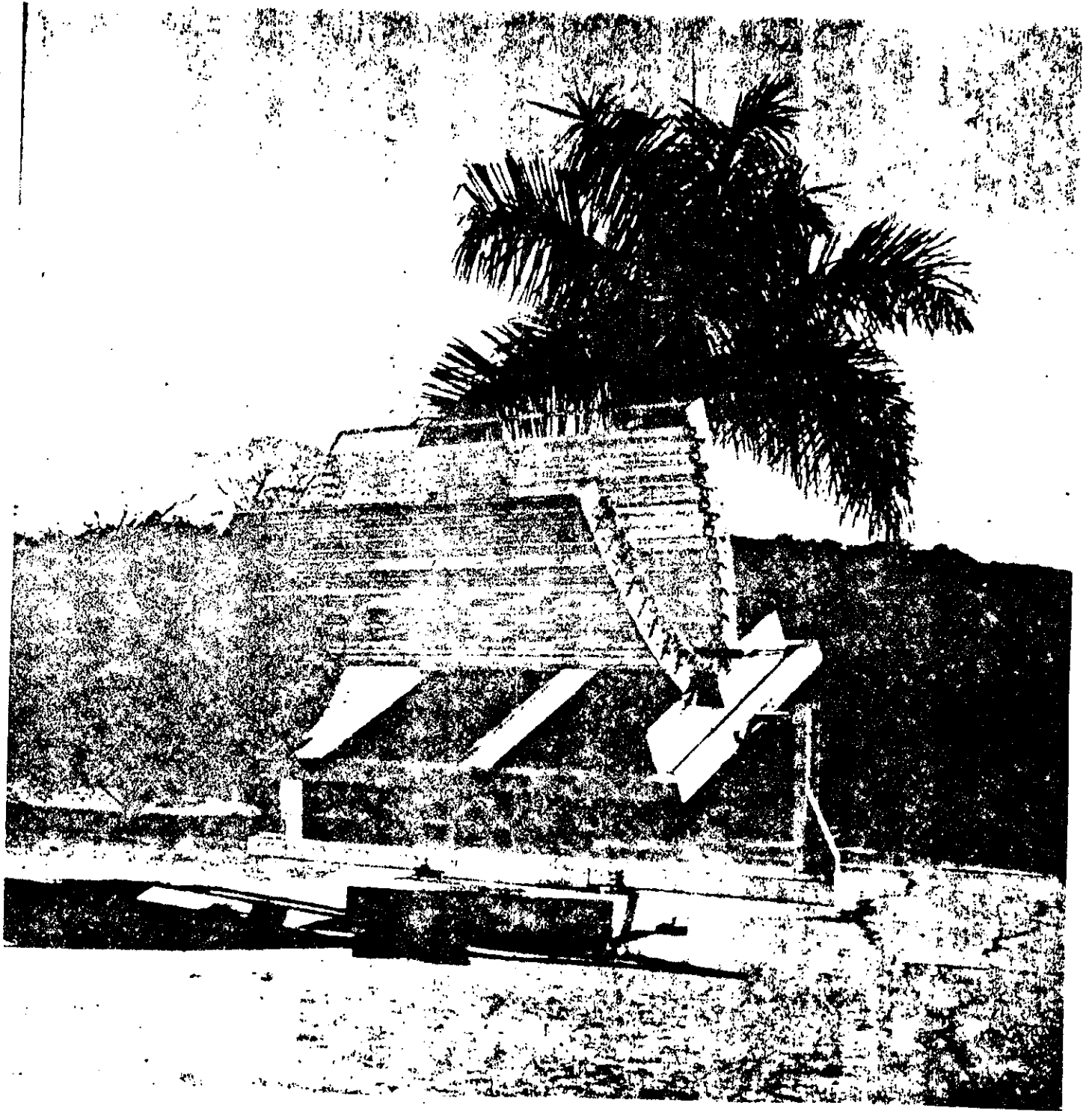


FIG. 14 COMPLETED BACARDÍ COLLECTOR

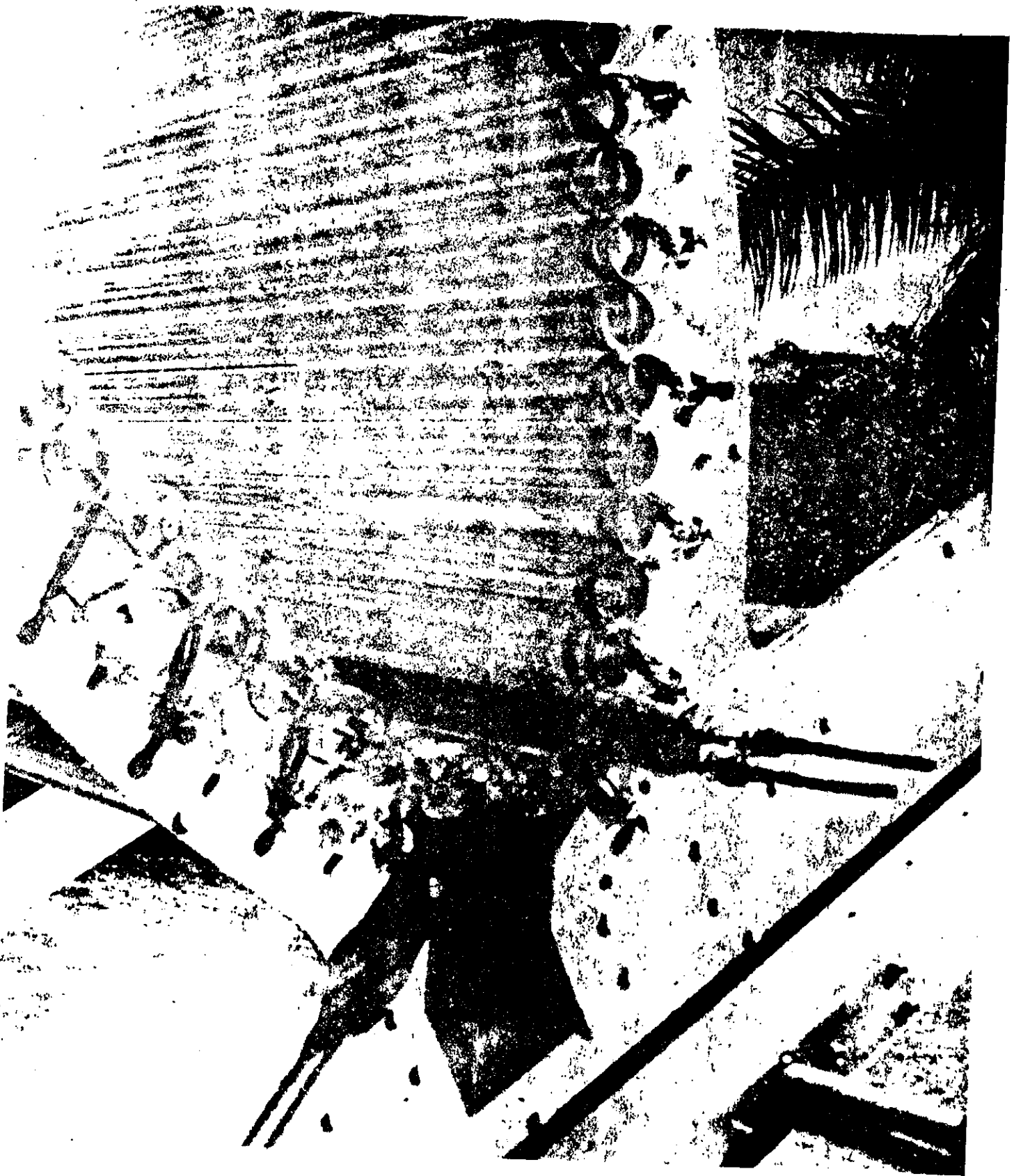


FIG. 15 COMPLETED BACARDÍ COLLECTOR. CLOSE-UP VIEW
OF ONE TUBE WELL AND RELATED SUPPORT
STRUCTURE.

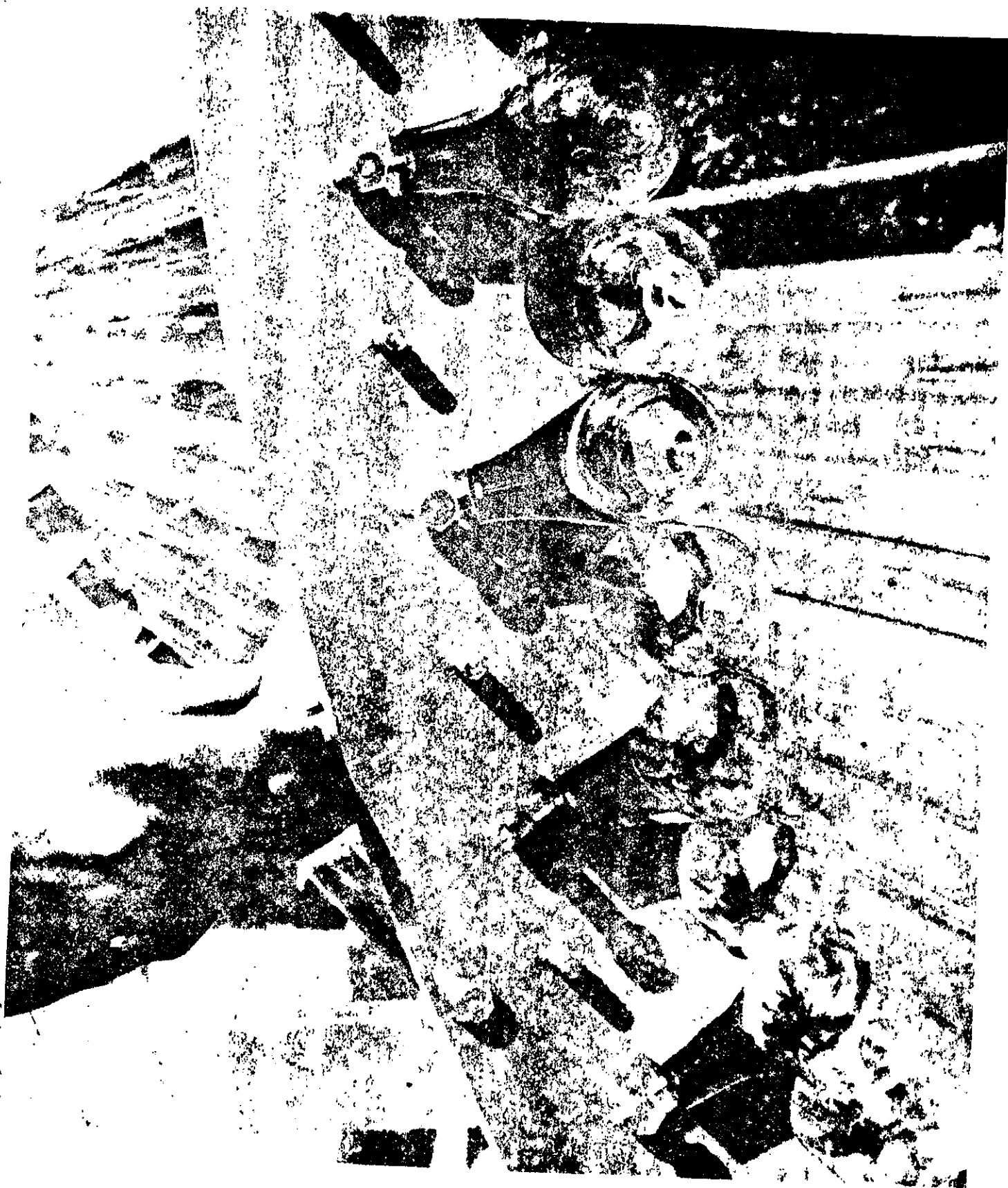


FIG. 16 COMPLETED BACARDÍ COLLECTOR, CLOSE-UP VIEW
OF ATTACHMENT OF MIRROR TUBES TO TUBE WELL.

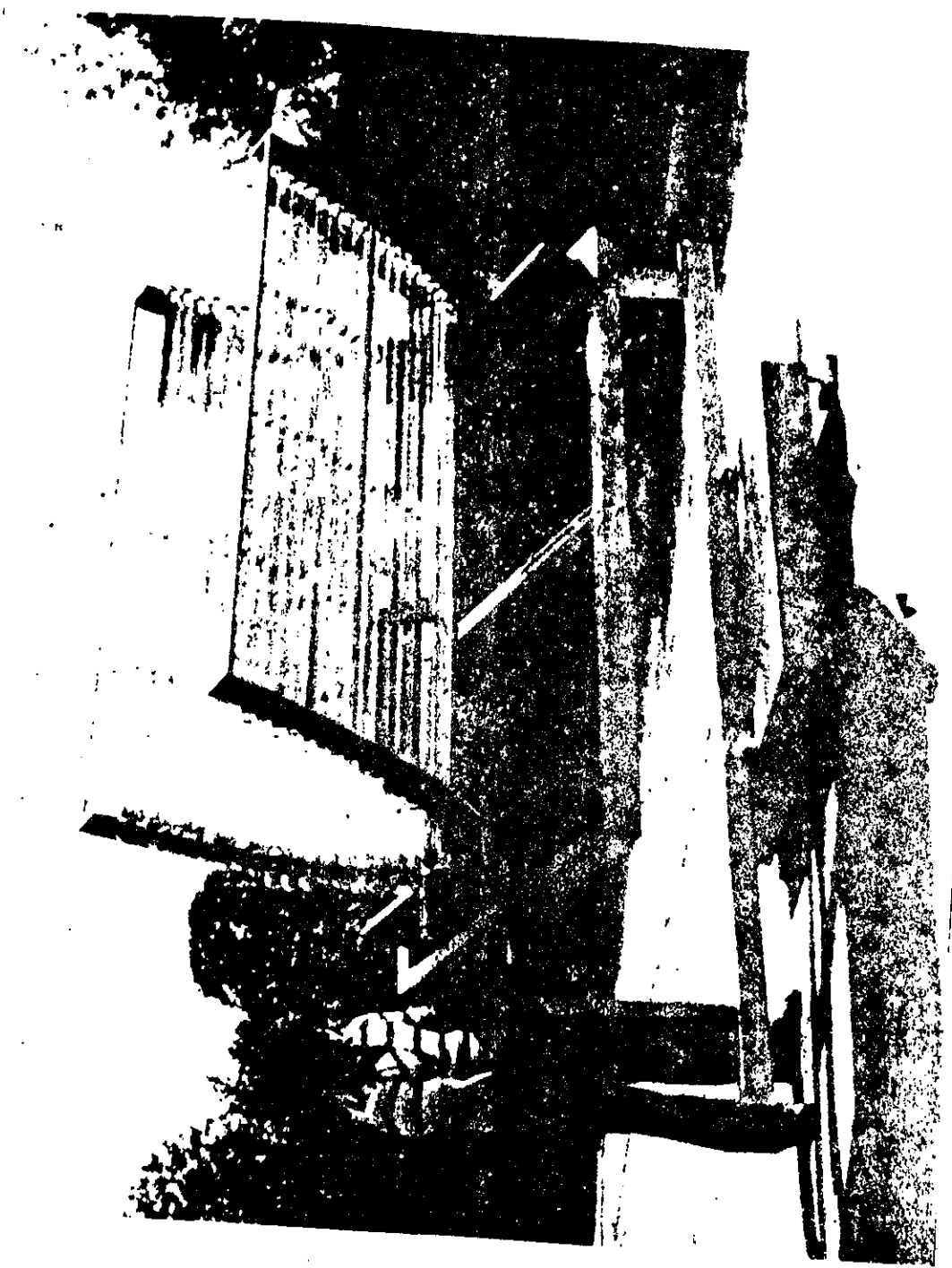


FIG. 17 COMPLETED BACARDÍ COLLECTOR. COLLECTOR
TILT IS ADJUSTED MANUALLY.

APPENDIX A

MONTHLY TOTAL SOLAR INSOLATION IN BTU/FI**2 VS. HOUR

MONTH: JUL 1978
 LOCATION: BACARUJ, CATAND
 0.00 3.00 6.00 9.00 12.00 15.00 18.00 21.00 24.00

Hour	0.00	3.00	6.00	9.00	12.00	15.00	18.00	21.00	24.00
350.00									
341.03									
332.05									
323.08									
314.10									
305.13									
296.15									
287.18									
278.21									
269.23									
260.26									
251.28									
242.31									
233.33									
224.36									
215.38									
206.41									
197.44									
188.46									
179.49									
170.51									
161.54									
152.56									
143.59									
134.62									
125.64									
116.67									
107.69									
98.72									
89.74									
80.77									
71.79									
62.82									
53.85									
44.87									
35.90									
26.92									
17.95									
8.97									
0.00									

0.00 3.00 6.00 9.00 12.00 15.00 18.00 21.00 24.00
 (+) MAXIMUM VALUE (M) MEAN VALUE (-) MINIMUM VALUE

FREQUENCY CHARTS FOR TOTAL / EXTRA-RESISTIAL INSULATION

MONTH: JUL 1978

LOCATION: SACANDU, CATAVU

BASED ON HOURLY VALUES

REGULAR

RANGE	0	20	40	60	80	100	120	NO. OF VALUES	% OF TOTAL
0-.1								1	0.39
.1-.2	XX							5	1.94
.2-.3	XXXXX							11	4.26
.3-.4	XXXXXXXXXX							22	8.53
.4-.5	XXXXXXXXXXXXXXXXXX							32	12.49
.5-.6	XXXXXXXXXXXXXXXXXXXXXX							37	14.34
.6-.7	XXXXXXXXXXXXXXXXXXXXXXXXXX							58	22.48
.7-.8	XXXXXXXXXXXXXXXXXXXXXXXXXXXXXX							87	33.72
.8-.9	XX							5	1.94
.9-1.								0	0.00

CUMULATIVE

RANGE	0	80	160	240	320	400	480	NO. OF VALUES	% OF TOTAL
0-.1								1	0.39
.1-.2	XX							6	2.33
.2-.3	XXXXX							17	6.59
.3-.4	XXXXXXXXXX							39	15.12
.4-.5	XXXXXXXXXXXXXXXXXX							71	27.52
.5-.6	XXXXXXXXXXXXXXXXXXXXXX							108	41.86
.6-.7	XXXXXXXXXXXXXXXXXXXXXXXXXX							166	64.34
.7-.8	XXXXXXXXXXXXXXXXXXXXXXXXXXXXXX							253	98.06
.8-.9	XX							258	100.00
.9-1.								258	100.00

BASED ON DAILY VALUES

REGULAR

RANGE	0	5	10	15	20	30	NO. OF VALUES	% OF TOTAL
0-.1							0	0.00
.1-.2							0	0.00
.2-.3							0	0.00
.3-.4							0	0.00
.4-.5	X						1	7.14
.5-.6	X						1	7.14
.6-.7	XXXXXXXXXX						9	64.29
.7-.8	XXX						3	21.43
.8-.9							0	0.00
.9-1.							0	0.00

CUMULATIVE

RANGE	0	10	20	30	NO. OF VALUES	% OF TOTAL
0-.1					0	0.00
.1-.2					0	0.00
.2-.3					0	0.00
.3-.4					0	0.00
.4-.5	X				1	7.14
.5-.6	XX				2	14.29
.6-.7	XXXXXXXXXX				11	78.57
.7-.8	XXXXXXXXXXXXXXXXXX				14	100.00
.8-.9	XXXXXXXXXXXXXXXXXX				14	100.00
.9-1.	XXXXXXXXXXXXXXXXXX				14	100.00

MONTHLY WEATHER DATA
 MONTH: JUL 1978
 LOCATION: MACAYUJ, GUATEMA
 DIFFUSE INSOLATION IN MJ/FT*2

DAY	6-7	7-8	8-9	9-10	10-11	11-12	12-1	HOJR	1-2	2-3	3-4	4-5	5-6	6-7	TOTAL
1	24.48	50.76	55.20	60.48	63.84	76.44	115.52	138.12	113.40	116.88	106.80	59.04	37.20	1419.2	
2	27.60	41.16	41.28	58.08	67.92	52.44	67.44	*****	50.04	46.92	77.16	57.72	27.04	*****	
3	29.08	67.80	102.72	97.80	*****	72.48	179.28	161.40	92.04	92.76	90.24	65.64	60.36	*****	
4	*****	77.64	90.00	99.00	132.00	113.04	108.72	119.28	110.08	111.36	81.72	80.00	33.36	*****	
5	30.84	78.36	69.12	87.48	81.96	125.74	125.04	*****	*****	*****	*****	*****	*****	*****	
6	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	
7	12.60	49.68	60.64	91.32	116.16	112.32	102.24	71.40	*****	55.56	50.16	31.68	12.24	*****	
8	48.24	52.32	85.92	140.76	144.48	156.48	155.88	173.16	*****	139.08	35.88	18.60	*****	*****	
9	15.12	45.60	85.92	77.52	87.60	79.32	103.80	95.64	*****	80.92	60.96	17.40	*****	*****	
10	15.24	53.40	46.68	75.00	56.20	68.04	56.76	62.16	*****	53.24	50.76	57.24	21.00	*****	
11	*****	44.40	42.60	46.44	48.12	141.24	160.92	98.88	*****	64.68	70.32	46.20	*****	*****	
12	32.76	46.92	68.40	88.92	97.28	92.40	118.44	103.44	96.24	*****	*****	*****	*****	*****	
13	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	
14	16.32	41.28	86.88	65.52	*****	46.44	54.00	50.40	*****	*****	77.28	57.84	*****	*****	
15	19.56	51.60	75.24	86.64	*****	*****	*****	*****	*****	62.52	73.44	57.96	11.88	*****	
16	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	
17	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	
18	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	
19	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	
20	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	
21	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	
22	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	
23	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	
24	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	
25	10.80	56.28	85.92	72.60	94.44	88.20	68.64	65.16	63.36	67.56	60.12	45.48	16.44	*****	
26	33.24	39.84	58.44	84.48	94.60	78.84	65.52	64.32	78.60	66.84	54.60	47.52	19.32	799.9	
27	7.92	38.04	84.60	84.36	96.36	91.92	83.40	70.68	65.04	62.84	72.24	45.36	15.36	781.7	
28	10.68	53.16	85.08	113.16	143.40	162.84	93.96	116.76	91.08	84.24	76.08	46.92	20.52	821.3	
29	22.32	47.04	81.12	95.40	102.12	100.20	112.92	109.20	106.56	109.92	76.12	50.64	17.40	1093.9	
30	11.52	49.20	79.28	102.36	96.12	102.12	91.60	109.32	78.84	75.72	73.56	45.72	33.48	1033.0	
31	8.04	45.48	72.00	122.16	130.68	135.24	111.72	92.28	71.28	48.36	59.16	34.32	17.28	948.6	

MEAN	STD D	MIN	MAX
16.13	47.48	75.26	91.88
9.36	6.27	12.18	20.57
7.92	58.04	55.20	60.48
33.24	56.28	85.92	122.16
72.20	143.40	162.84	116.52
158.12	113.40	116.88	106.80
47.51	72.59	78.80	83.52
6.94	16.55	23.83	18.61
34.32	54.60	48.36	64.32
59.04	106.80	116.88	113.40
37.20	22.14	8.36	47.51
647.8	68.0	6.94	6.94
1291.8	37.20	15.36	34.32

MONTHLY WEATHER DATA
 LOCATION: BACARDI, LAJANO

MONTH: JUL 1974

DIFFUSE / TOTAL INSULATION

DAY	HOUR (CODE)												L-7 (L)	L-7 VALUE
	6-7 (A)	7-8 (B)	8-9 (C)	9-10 (D)	10-11 (E)	11-12 (F)	12-1 (N)	1-2 (G)	2-3 (H)	3-4 (I)	4-5 (J)	5-6 (K)		
1	0.877	0.551	0.361	0.280	0.239	0.254	0.378	0.549	0.464	0.520	0.568	0.671	0.953	0.412
2	0.819	0.353	0.234	0.308	0.237	0.170	0.197	0.549	0.172	0.200	0.468	0.520	0.953	0.412
3	0.734	0.675	0.656	0.524	0.483	0.732	0.732	0.755	0.926	0.672	0.548	0.602	0.953	0.412
4	0.734	0.805	0.567	0.486	0.483	0.355	0.339	0.386	0.405	0.506	0.543	0.602	0.953	0.412
5	0.734	0.745	0.376	0.402	0.334	0.395	0.675	0.549	0.405	0.506	0.543	0.602	0.953	0.412
6	0.977	0.797	0.455	0.712	0.565	0.741	0.354	0.266	0.368	0.455	0.568	0.602	0.953	0.412
7	1.914	1.104	1.086	0.963	0.663	0.809	0.790	0.635	0.368	0.455	0.568	0.602	0.953	0.412
8	0.752	0.598	0.549	0.363	0.327	0.270	0.357	0.318	0.368	0.455	0.568	0.602	0.953	0.412
9	0.833	0.638	0.320	0.330	0.210	0.226	0.178	0.212	0.368	0.455	0.568	0.602	0.953	0.412
10	0.833	0.535	0.263	0.201	0.170	0.226	0.178	0.212	0.368	0.455	0.568	0.602	0.953	0.412
11	1.040	0.611	0.550	0.677	0.355	0.313	0.414	0.408	0.368	0.455	0.568	0.602	0.953	0.412
12	0.877	0.911	0.512	0.290	0.355	0.313	0.414	0.408	0.368	0.455	0.568	0.602	0.953	0.412
13	0.798	0.603	0.580	0.503	0.355	0.313	0.414	0.408	0.368	0.455	0.568	0.602	0.953	0.412
14	0.877	0.911	0.512	0.290	0.355	0.313	0.414	0.408	0.368	0.455	0.568	0.602	0.953	0.412
15	0.798	0.603	0.580	0.503	0.355	0.313	0.414	0.408	0.368	0.455	0.568	0.602	0.953	0.412
16	0.877	0.911	0.512	0.290	0.355	0.313	0.414	0.408	0.368	0.455	0.568	0.602	0.953	0.412
17	0.877	0.911	0.512	0.290	0.355	0.313	0.414	0.408	0.368	0.455	0.568	0.602	0.953	0.412
18	0.877	0.911	0.512	0.290	0.355	0.313	0.414	0.408	0.368	0.455	0.568	0.602	0.953	0.412
19	0.877	0.911	0.512	0.290	0.355	0.313	0.414	0.408	0.368	0.455	0.568	0.602	0.953	0.412
20	0.877	0.911	0.512	0.290	0.355	0.313	0.414	0.408	0.368	0.455	0.568	0.602	0.953	0.412
21	0.877	0.911	0.512	0.290	0.355	0.313	0.414	0.408	0.368	0.455	0.568	0.602	0.953	0.412
22	0.877	0.911	0.512	0.290	0.355	0.313	0.414	0.408	0.368	0.455	0.568	0.602	0.953	0.412
23	0.877	0.911	0.512	0.290	0.355	0.313	0.414	0.408	0.368	0.455	0.568	0.602	0.953	0.412
24	0.877	0.911	0.512	0.290	0.355	0.313	0.414	0.408	0.368	0.455	0.568	0.602	0.953	0.412
25	0.837	0.630	0.640	0.465	0.350	0.299	0.220	0.215	0.236	0.304	0.413	0.635	1.015	0.350
26	0.969	0.572	0.471	0.746	0.364	0.256	0.209	0.213	0.262	0.310	0.374	0.616	0.976	0.347
27	0.800	0.755	0.562	0.390	0.347	0.306	0.265	0.238	0.243	0.286	0.469	0.532	0.977	0.349
28	0.791	0.936	0.732	0.628	0.608	0.557	0.312	0.388	0.351	0.410	0.553	0.681	1.097	0.501
29	0.872	0.784	0.590	0.471	0.397	0.345	0.371	0.380	0.421	0.526	0.596	0.890	1.061	0.463
30	0.841	0.772	0.661	0.479	0.364	0.337	0.300	0.458	0.303	0.368	0.541	0.630	1.154	0.426
31	0.522	0.699	0.551	0.689	0.555	0.737	0.390	0.314	0.259	0.222	0.368	0.450	1.054	0.445
MEAN	0.805	0.764	0.661	0.553	0.426	0.405	0.296	0.315	0.249	0.347	0.474	0.630	1.031	0.412
STD D	0.138	0.112	0.085	0.134	0.108	0.175	0.070	0.097	0.066	0.099	0.092	0.136	0.286	0.065
MIN	0.522	0.572	0.471	0.390	0.347	0.256	0.219	0.213	0.236	0.222	0.368	0.450	0.890	0.347
MAX	0.969	0.936	0.732	0.746	0.608	0.737	0.390	0.458	0.421	0.526	0.596	0.890	1.154	0.501

FREQUENCY CHART FOR OFFUSE / TOTAL INSOLATION

MONTH: JUL 1978

LOCATION: SACARU, CATAMU

BASED ON HOURLY VALUES

REGULAR

RANGE	0	20	40	60	80	100	120	NO. OF VALUES	% OF TOTAL
0-.1								0	0.00
.1-.2		XXXX						9	3.93
.2-.3		XXXXXXXXXXXXXXXXXXXX						30	13.10
.3-.4		XXXXXXXXXXXXXXXXXXXX						45	19.65
.4-.5		XXXXXXXXXXXXXXXXXXXX						23	10.04
.5-.6		XXXXXXXXXXXXXXXXXXXX						26	11.35
.6-.7		XXXXXXXXXXXXXXXXXXXX						18	7.86
.7-.8		XXXXXXXXXX						15	6.55
.8-.9		XXXXXX						10	4.37
.9-1.									

THERE ARE 20 VALUES ABOVE 1.0 (8.73%)

CUMULATIVE

RANGE	0	80	160	240	320	400	480	NO. OF VALUES	% OF TOTAL
0-.1								0	0.00
.1-.2	X							9	3.93
.2-.3	XXXX							39	17.03
.3-.4	XXXXXXXXXXXX							64	36.68
.4-.5	XXXXXXXXXXXXXXXXXXXX							107	46.72
.5-.6	XXXXXXXXXXXXXXXXXXXX							140	61.14
.6-.7	XXXXXXXXXXXXXXXXXXXX							166	72.49
.7-.8	XXXXXXXXXXXXXXXXXXXX							184	80.55
.8-.9	XXXXXXXXXXXXXXXXXXXX							199	86.90
.9-1.	XXXXXXXXXXXXXXXXXXXX							209	91.27

BASED ON DAILY VALUES

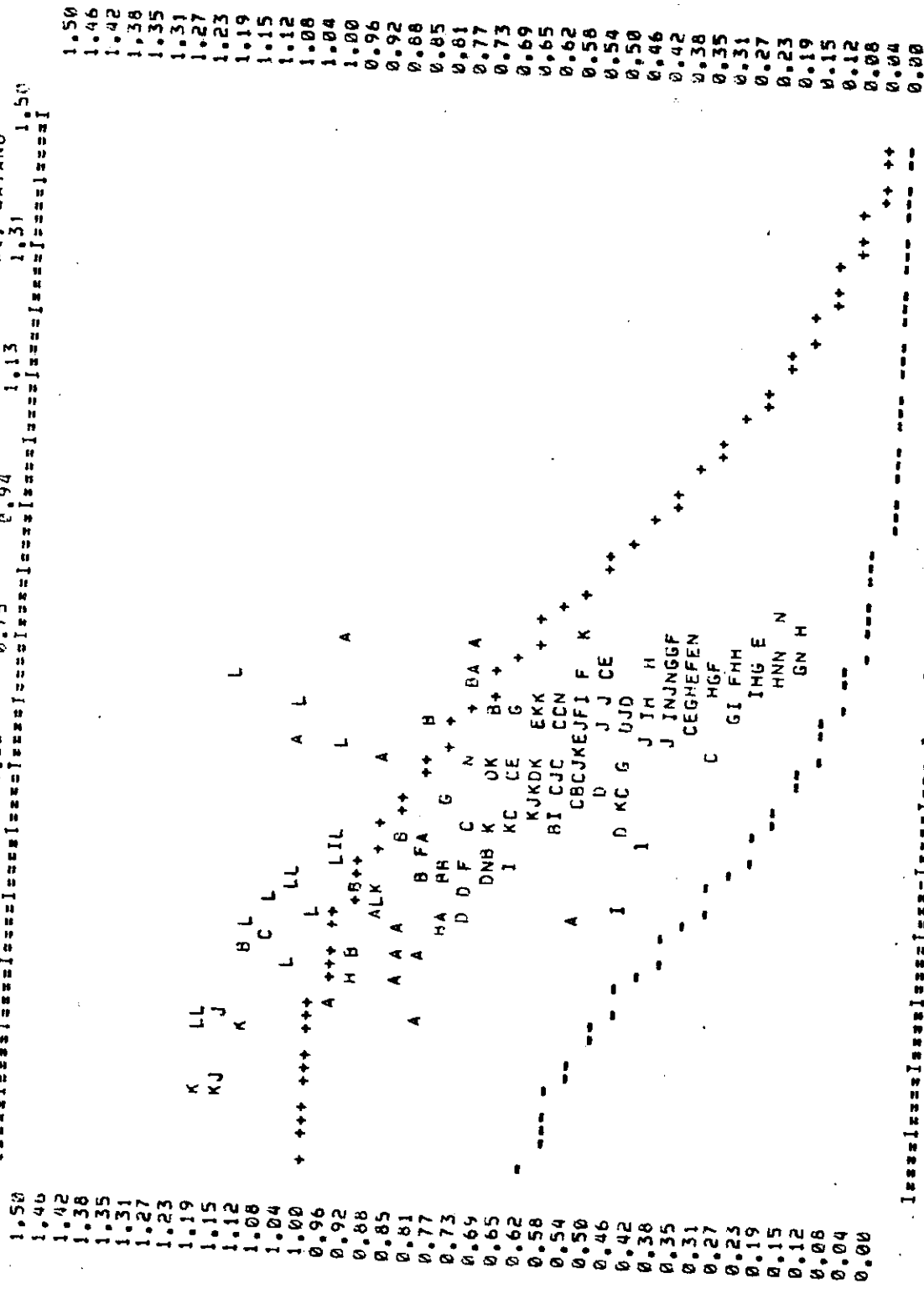
REGULAR

CUMULATIVE

RANGE	0	5	10	15	20	30	NO. OF VALUES	% OF TOTAL
0-.1							0	0.00
.1-.2							0	0.00
.2-.3		XXX					0	0.00
.3-.4		XXX					0	0.00
.4-.5		X					3	42.86
.5-.6							3	42.86
.6-.7							1	14.29
.7-.8							0	0.00
.8-.9							0	0.00
.9-1.							0	0.00

TOTAL / EXTRATERRESTIAL INSOLATION (HORIZONTAL AXIS)
 VS. DIFFUSE / TOTAL INSOLATION (VERTICAL AXIS)

MONTH: JUL 1978
 0.00 0.19 0.38 0.56 0.75 0.94 1.13 1.31 1.50
 LOCATION: SACARDI, CATANO



FOR LETTER CODES SEE TOTAL / EXTRATERRESTIAL INSOLATION TABLE OR DIFFUSE / TOTAL INSOLATION TABLE
 (+) MAXIMUM VALUE CURVE POINTS (-) MINIMUM VALUE CURVE POINTS

KT: TOTAL / EXTRATERRESTIAL *** 145 VALUES ABOVE 1.5 *** 145 VALUES WITHOUT DATA
 KD: DIFFUSE / TOTAL *** 175 VALUES ABOVE 1.5 *** 174 VALUES WITHOUT DATA

MONTHLY WEATHER DATA

MONTH: AUG 1978

LOCATION: BANGOR, LAFA 01

TOTAL INSOLATION IN HOURS**

DAY	6-7	7-8	8-9	9-10	10-11	11-12	12-1	1-2	2-3	3-4	4-5	5-6	6-7	TOTAL
1	18.10	58.10	68.40	116.80	161.10	246.50	207.80	104.50	99.60	68.00	63.30	47.20	21.40	1301.0
2	19.70	69.80	120.60	210.80	267.30	302.00	314.40	301.70	276.10	219.40	104.40	33.10	20.40	2249.7
3	6.20	23.40	64.50	127.70	228.50	277.40	208.20	161.00	155.50	98.50	61.20	46.20	34.10	1490.2
4	11.10	57.40	113.10	143.30	141.50	194.10	213.30	231.20	242.50	181.80	147.70	42.60	12.50	1731.9
5	14.40	70.10	149.90	188.10	272.80	268.00	305.20	259.40	273.90	224.50	138.00	60.40	15.00	2259.5
6	26.70	72.20	155.30	226.60	266.40	315.50	322.80	347.50	294.10	216.40	155.60	90.50	15.10	2468.7
7	18.80	86.50	103.40	205.40	251.80	73.40	104.20	52.00	24.00	48.10	72.10	51.10	11.00	1101.8
8	29.40	80.30	162.50	152.50	265.30	309.70	322.40	323.70	259.90	180.30	76.50	71.60	14.20	2268.3
9	19.60	74.70	159.90	192.30	273.30	308.60	187.20	12.50	*****	*****	*****	*****	*****	*****
10	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
11	14.00	65.80	126.00	208.00	257.30	301.00	316.20	306.10	276.40	216.80	149.10	77.20	12.60	*****
12	23.60	66.90	97.10	214.00	270.80	304.70	319.80	314.40	279.10	222.50	154.80	79.20	15.90	2332.8
13	14.60	73.30	136.60	219.70	268.60	310.90	300.90	321.50	274.90	222.40	156.50	66.50	14.30	2369.5
14	9.70	44.50	56.40	102.40	224.50	173.00	143.00	125.50	80.30	55.50	32.60	93.10	13.20	2406.2
15	13.90	41.60	87.20	181.70	250.40	290.40	307.80	299.90	251.40	202.90	121.60	27.60	4.70	1890.3
16	12.70	43.70	37.60	64.90	32.90	10.80	9.10	20.00	29.70	32.30	24.70	26.20	9.00	2124.6
17	17.70	25.30	48.50	93.40	106.50	126.60	127.10	126.50	*****	39.10	41.50	8.50	2.60	329.9
18	17.60	72.90	124.70	133.00	181.10	229.00	243.80	157.30	74.30	47.60	43.80	54.80	10.50	*****
19	12.70	89.40	142.50	156.30	225.80	261.40	235.20	184.80	192.50	200.50	126.40	24.80	6.40	1356.3
20	20.60	69.20	135.70	129.50	275.60	290.50	307.70	307.70	279.10	213.30	115.10	45.80	6.40	1770.2
21	10.60	71.10	110.40	127.10	149.30	175.40	290.70	302.40	264.60	*****	*****	45.20	11.10	2209.3
22	14.00	68.80	130.30	203.50	147.40	75.00	214.80	114.30	91.60	166.30	121.50	45.30	*****	*****
23	*****	66.80	130.40	154.70	262.60	281.70	269.10	231.80	255.50	194.50	100.00	36.90	9.00	*****
24	22.20	60.50	130.70	204.00	267.50	300.70	310.30	293.10	255.30	195.90	132.20	57.60	6.10	2236.1
25	14.40	70.50	130.10	217.10	275.50	306.70	310.50	302.90	265.00	203.00	69.40	75.40	7.20	2255.7
26	21.50	53.80	126.00	221.40	275.30	304.10	311.20	296.30	259.00	202.00	117.60	22.60	3.00	2213.8
27	15.20	68.60	151.00	92.90	158.10	146.50	171.30	163.60	173.20	184.10	112.00	44.60	4.20	1485.3
28	13.20	67.20	140.40	177.00	211.50	297.80	306.00	266.50	247.70	191.20	122.00	50.80	5.50	2116.8
29	12.80	66.90	140.20	205.10	264.00	296.50	305.40	289.10	251.50	195.10	126.70	52.50	5.90	2211.7
30	13.30	68.90	148.90	217.70	268.20	303.00	315.40	158.90	41.30	49.60	35.10	18.80	3.10	1642.2
31	15.30	74.70	150.00	219.10	272.80	295.60	319.60	300.20	262.30	181.10	109.70	31.10	3.90	2235.4

MEAN
STD D
MIN
MAX

16.44	66.35	121.51	174.56	230.85	250.66	255.42	230.12	200.32	162.27	103.68	49.17	10.42	1071.7
5.14	13.86	32.02	47.07	60.21	85.81	85.07	92.89	91.25	67.51	41.50	22.73	6.08	213.3
8.00	23.40	37.60	64.90	32.90	10.80	9.10	20.00	24.00	32.30	24.70	8.50	2.80	299.2
29.40	89.40	162.50	226.60	285.30	319.50	322.80	323.70	294.10	224.30	156.50	93.10	30.10	2557.3

FREQUENCY CHARTS FOR TOTAL / EXTRATE-RESISTAL INSULATION

MONTH: AUG 1976

LOCATION: SACARDI, CATAND

BASED ON DAILY VALUES

REGULAR

RANGE	0	20	40	60	80	100	120	NO. OF VALUES	% OF TOTAL
0-.1	X							8	2.09
.1-.2	XXXX	XXXXXXXXXX						25	6.54
.2-.3	XXXXXXXXXX	XXXXXXXXXX						29	7.59
.3-.4	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX					47	12.30
.4-.5	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX				55	14.40
.5-.6	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX			56	14.66
.6-.7	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX		61	15.97
.7-.8	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	98	25.65
.8-.9	X							3	0.79
.9-1.								0	0.00

CUMULATIVE

RANGE	0	80	160	240	320	400	480	NO. OF VALUES	% OF TOTAL
0-.1	X							8	2.09
.1-.2	XXXX	XXXXXXXXXX						33	8.54
.2-.3	XXXXXXXXXX	XXXXXXXXXX						62	16.23
.3-.4	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX					109	28.53
.4-.5	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX				164	42.93
.5-.6	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX			220	57.59
.6-.7	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX		281	73.56
.7-.8	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	379	99.21
.8-.9	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	382	100.00
.9-1.								382	100.00

BASED ON DAILY VALUES

REGULAR

RANGE	0	5	10	15	NO. OF VALUES	% OF TOTAL	0	10	20	30	NO. OF VALUES	% OF TOTAL
0-.1	X				1	3.85	X				1	3.85
.1-.2					0	0.00	X				1	3.85
.2-.3					0	0.00	X				1	3.85
.3-.4	XXX				3	11.54	XXXX				4	15.38
.4-.5	XXXX				4	15.38	XXXXXXXXXX				8	30.77
.5-.6	XXX				3	11.54	XXXXXXXXXX				11	42.31
.6-.7	XXXXXXXXXXXX				12	46.15	XXXXXXXXXXXX				23	68.46
.7-.8	XXX				3	11.54	XXXXXXXXXXXX				26	100.00
.8-.9					0	0.00	XXXXXXXXXXXX				26	100.00
.9-1.					0	0.00	XXXXXXXXXXXX				26	100.00

CUMULATIVE

MONTH: AUG 1978
 MONTHLY WEATHER DATA
 LOCATION: MACARU, CALAHO
 DIFFUSE INSOLATION IN HOURS

DAY	6-7	7-8	8-9	9-10	10-11	11-12	12-1	1-2	2-3	3-4	4-5	5-6	6-7	TOTAL
1	*****	42.83	83.01	87.60	105.63	178.23	116.28	43.65	96.61	72.24	61.71	49.13	19.48	*****
2	15.25	32.67	57.23	66.19	66.43	68.97	65.70	62.68	62.07	60.14	58.34	34.61	23.47	665.7
3	2.66	22.63	53.60	78.41	101.52	132.13	160.74	147.74	138.30	104.00	63.64	47.92	26.02	1265.4
4	6.95	53.84	95.71	130.80	139.15	174.18	185.86	194.57	163.83	109.75	100.77	44.16	10.77	1411.9
5	11.62	34.85	67.88	85.06	89.06	99.46	85.55	100.60	90.27	82.04	64.73	42.95	17.18	577.3
6	25.05	47.79	75.87	82.88	65.10	73.57	63.89	72.96	75.02	55.57	39.69	44.29	13.19	714.9
7	11.74	30.85	32.79	48.52	57.60	52.86	102.49	56.00	25.77	49.51	84.34	45.86	*****	*****
8	24.68	54.00	53.36	88.57	52.03	51.42	43.08	60.02	54.69	98.61	72.96	59.17	*****	*****
9	14.88	24.44	57.96	98.37	62.92	52.15	56.14	74.17	*****	*****	*****	*****	*****	*****
10	*****	37.75	52.03	56.51	62.19	55.33	51.67	49.13	47.79	48.04	47.55	32.19	14.77	*****
11	24.08	37.03	54.33	50.34	45.74	44.89	43.80	40.90	39.81	34.24	32.67	32.43	13.91	572.1
12	6.78	17.54	43.20	39.81	40.05	72.84	50.94	41.62	31.82	33.64	26.01	39.78	12.22	493.1
13	6.23	28.92	37.51	59.41	89.54	113.98	107.45	169.02	89.90	53.48	33.52	25.65	13.67	456.4
14	10.89	54.21	79.38	92.93	84.15	79.38	69.82	67.76	76.84	66.91	67.76	22.99	*****	*****
15	12.95	34.73	35.82	63.77	34.73	11.25	9.56	19.24	30.85	31.40	26.26	9.07	2.66	786.5
16	20.93	21.90	44.77	87.24	105.15	120.03	120.03	118.34	*****	39.06	41.02	35.45	*****	322.3
17	11.62	27.35	37.99	70.91	110.35	121.24	159.36	144.23	84.09	48.88	48.28	26.74	*****	*****
18	9.68	37.63	29.16	57.23	83.01	78.04	50.70	83.49	85.30	64.25	71.27	31.94	7.30	689.1
19	14.64	24.32	35.33	67.15	53.60	51.67	52.39	53.82	51.67	40.90	49.85	44.65	12.95	549.9
20	5.01	37.51	41.14	104.42	112.77	153.14	164.00	92.93	128.38	*****	*****	*****	*****	*****
21	10.77	36.30	54.09	91.60	111.68	64.37	125.11	99.46	79.15	88.57	73.57	38.40	6.53	879.7
22	37.51	35.57	57.35	94.50	93.29	91.96	96.32	101.03	94.26	81.67	58.44	28.43	9.32	879.7
23	21.30	32.79	52.15	58.20	60.86	59.77	60.17	59.17	55.90	50.21	43.54	28.07	6.05	568.2
24	8.11	20.93	36.78	44.29	38.72	35.09	34.36	31.74	29.52	32.91	43.92	39.61	7.06	404.0
25	14.04	27.47	50.34	47.79	47.79	46.83	50.82	46.04	44.77	38.11	30.25	18.63	5.51	468.4
26	8.47	23.84	50.09	91.35	115.55	132.74	148.10	134.79	131.28	104.79	63.28	33.40	4.84	1042.5
27	9.68	34.36	52.03	69.45	79.74	71.87	76.11	77.20	74.66	65.10	51.67	32.19	6.05	700.1
28	6.95	32.91	53.84	65.34	67.64	70.06	71.15	69.09	61.35	54.21	47.07	29.77	6.41	637.7
29	8.71	27.10	49.25	54.93	54.45	54.21	59.77	54.57	40.41	49.73	35.33	18.75	3.03	510.9
30	6.78	15.37	21.30	25.29	50.94	51.91	37.27	34.97	30.98	38.48	30.60	18.75	4.11	374.7
31	13.16	32.80	52.58	66.61	72.15	73.67	75.20	74.06	69.61	59.76	51.13	32.60	10.18	686.8
MEAN	7.79	10.27	16.72	23.32	27.76	35.89	44.17	42.15	36.76	25.33	18.01	10.22	6.29	96.1
STD D	2.66	15.37	21.30	25.29	34.73	11.25	9.56	19.24	29.52	31.46	26.01	9.07	2.66	236.1
MIN	37.51	54.21	95.71	130.80	139.15	174.48	185.86	194.57	163.83	109.75	100.07	47.92	26.02	1460.5
MAX	15.25	42.83	83.01	87.60	105.63	178.23	116.28	43.65	96.61	72.24	61.71	49.13	19.48	*****

MONTHLY DIFFUSE INSULATION IN MJU/FT**2 VS. HOUR

MONTH: AUG 1978	6.00	9.00	12.00	15.00	18.00	21.00	24.00
350.00							
341.03							
332.05							
323.08							
314.10							
305.13							
296.15							
287.18							
278.21							
269.23							
260.26							
251.28							
242.31							
233.33							
224.36							
215.39							
206.41							
197.44							
188.46							
179.49							
170.51							
161.54							
152.56							
143.59							
134.62							
125.64							
116.67							
107.69							
98.72							
89.74							
80.77							
71.79							
62.82							
53.85							
44.87							
35.90							
26.92							
17.95							
8.97							
0.00							

0.00 3.00 6.00 9.00 12.00 15.00 18.00 21.00 24.00
 (S) MEAN VALUE PLUS OR MINUS STD O (M) MEAN VALUE

MONTHLY WEATHER DATA

MONTH: AUG 1976

LOCATION: MACAMBI, BRAZIL

DIFFUSE / TOTAL INSOLATION

DAY	MOOR (COLE)														DAILY VALUE
	6-7 (A)	7-8 (B)	8-9 (C)	9-10 (D)	10-11 (E)	11-12 (F)	12-1 (N)	1-2 (G)	2-3 (H)	3-4 (I)	4-7 (J)	5-6 (K)	6-7 (L)		
1	0.774	0.737	0.939	0.750	0.656	0.723	0.560	0.096	0.984	1.062	0.975	1.041	0.910	*****	
2	0.333	0.468	0.475	0.314	0.249	0.228	0.212	0.230	0.231	0.274	0.482	1.045	1.151	0.290	
3	0.607	0.938	0.831	0.614	0.440	0.476	0.801	0.910	0.809	1.050	1.030	1.037	0.864	0.720	
4	0.807	0.497	0.453	0.452	0.983	0.899	0.871	0.842	0.676	0.674	0.678	1.037	0.862	0.815	
5	0.938	0.662	0.489	0.366	0.326	0.345	0.280	0.411	0.330	0.360	0.469	0.711	1.145	0.380	
6	0.624	0.357	0.317	0.236	0.244	0.230	0.190	0.237	0.255	0.164	0.255	0.489	0.873	0.290	
7	0.840	0.423	0.328	0.581	0.182	0.166	0.984	1.117	1.074	1.031	1.170	0.097	*****	*****	
8	0.759	0.327	0.362	0.512	0.230	0.169	0.134	0.185	0.210	0.547	0.954	0.026	*****	*****	
9	*****	*****	*****	*****	*****	*****	0.300	1.023	*****	*****	*****	*****	*****	*****	
10	0.864	0.574	0.413	0.272	0.242	0.184	0.163	0.160	0.175	0.222	0.290	0.417	0.855	*****	
11	1.046	0.553	0.560	0.235	0.169	0.147	0.137	0.130	0.143	0.154	0.319	0.461	0.875	0.245	
12	0.464	0.239	0.316	0.181	0.149	0.234	0.109	0.128	0.116	0.151	0.106	0.375	0.625	0.200	
13	0.848	0.650	0.642	0.580	0.399	0.659	0.748	0.869	1.018	0.964	1.028	0.420	1.036	0.190	
14	0.783	0.664	0.910	0.511	0.344	0.273	0.227	0.220	0.305	0.330	0.557	0.929	*****	*****	
15	1.019	0.795	0.948	0.983	1.056	1.042	1.050	0.962	1.059	0.974	1.003	0.877	1.197	0.370	
16	1.183	0.866	0.923	0.934	0.987	0.948	0.944	0.935	*****	*****	1.003	1.066	0.951	0.977	
17	0.660	0.375	0.305	0.533	0.609	0.529	0.654	0.917	1.132	1.000	0.988	1.019	*****	*****	
18	0.762	0.421	0.205	0.360	0.366	0.299	0.425	0.915	1.132	1.027	1.102	1.078	*****	*****	
19	0.711	0.351	0.260	0.519	0.194	0.173	0.170	0.452	0.443	0.320	0.564	0.697	1.070	0.389	
20	0.548	0.528	0.373	0.822	0.755	0.873	0.567	0.165	0.165	0.192	0.433	0.988	1.106	0.249	
21	0.769	0.528	0.391	0.450	0.750	0.873	0.567	0.307	0.485	*****	*****	*****	*****	*****	
22	0.959	0.533	0.440	0.611	0.355	0.854	0.582	0.670	0.864	0.533	0.645	0.049	0.803	0.523	
23	0.563	0.297	0.399	0.285	0.228	0.324	0.358	0.436	0.369	0.420	0.548	0.771	1.035	*****	
24	0.653	0.511	0.283	0.204	0.141	0.194	0.194	0.202	0.219	0.250	0.330	0.487	0.992	0.405	
25	0.557	0.547	0.349	0.216	0.174	0.154	0.106	0.105	0.111	0.102	0.533	0.520	1.092	0.179	
26	0.733	0.511	0.332	0.983	0.731	0.906	0.103	0.162	0.173	0.189	0.257	0.525	1.170	0.214	
27	0.733	0.511	0.371	0.392	0.377	0.241	0.249	0.820	0.758	0.560	0.505	0.749	1.152	0.702	
28	0.700	0.492	0.384	0.319	0.256	0.236	0.233	0.269	0.301	0.340	0.423	0.634	1.111	0.331	
29	0.655	0.393	0.331	0.252	0.203	0.236	0.233	0.239	0.244	0.278	0.371	0.567	1.087	0.280	
30	0.445	0.206	0.142	0.115	0.107	0.179	0.190	0.303	0.979	1.003	1.007	0.996	1.171	0.311	
31	0.731	0.522	0.464	0.426	0.372	0.362	0.117	0.116	0.118	0.212	1.352	0.003	1.035	1.100	
MEAN	0.167	0.201	0.230	0.255	0.273	0.293	0.352	0.379	0.407	0.390	0.512	0.736	1.037	0.392	
STD D	0.333	0.206	0.142	0.115	0.141	0.114	0.106	0.303	0.316	0.289	0.260	0.232	0.123	0.235	
MIN	1.046	0.967	0.948	0.983	1.056	1.042	1.050	0.962	0.111	0.151	0.106	0.375	0.855	0.100	
MAX	0.731	0.522	0.464	0.426	0.372	0.362	0.352	0.379	0.407	0.390	0.512	0.736	1.037	0.392	

FREQUENCY CHARTS FOR DIFFUSE / T I-L I-REGULATION

MONTH: AUG 1978

LOCATION: KILGARI, CANADA

BASED ON HOURLY VALUES

REGULAR

RANGE	20	40	60	80	100	120	NO. OF VALUES	% OF TOTAL
0-.1							4	0.02
.1-.2	XXXXXXXXXXXXXXXXXXXX						53	14.10
.2-.3	XXXXXXXXXXXXXXXXXXXX						54	14.36
.3-.4	XXXXXXXXXXXXXXXXXXXX						49	13.03
.4-.5	XXXXXXXXXXXXXXXXXXXX						32	8.51
.5-.6	XXXXXXXXXXXXXXXXXXXX						31	8.24
.6-.7	XXXXXXXXXXXX						23	6.12
.7-.8	XXXXXXXXXXXX						20	5.52
.8-.9	XXXXXXXXXXXX						34	9.04
.9-1.	XXXXXXXXXXXX						36	9.57
THERE ARE 44 VALUES ABOVE 1.0 (11.70%)								

CUMULATIVE

RANGE	0	80	160	240	320	400	480	NO. OF VALUES	% OF TOTAL
0-.1								0	0.00
.1-.2	XXXXXX							53	14.10
.2-.3	XXXXXXXXXXXXXXXXXXXX							107	28.46
.3-.4	XXXXXXXXXXXXXXXXXXXX							156	41.49
.4-.5	XXXXXXXXXXXXXXXXXXXX							188	50.00
.5-.6	XXXXXXXXXXXXXXXXXXXX							219	58.24
.6-.7	XXXXXXXXXXXXXXXXXXXX							242	64.36
.7-.8	XXXXXXXXXXXXXXXXXXXX							262	69.68
.8-.9	XXXXXXXXXXXXXXXXXXXX							296	78.72
.9-1.	XXXXXXXXXXXXXXXXXXXX							332	88.30

BASED ON DAILY VALUES

REGULAR

RANGE	0	5	10	15	20	25	30	NO. OF VALUES	% OF TOTAL
0-.1								0	0.00
.1-.2	XXX							3	14.29
.2-.3	XXXXXXXXXX							11	52.38
.3-.4	XXXXX							16	76.19
.4-.5								16	76.19
.5-.6								16	76.19
.6-.7	X							17	80.95
.7-.8	XX							19	90.46
.8-.9	X							20	95.24
.9-1.	X							21	100.00

CUMULATIVE

MONTHLY WEATHER DATA

STATION: SLP 1978

LOCATION: SACAPUJ, CATAGU

TOTAL INSOLATION IN HOURS

DAY	0-7	7-8	8-9	9-10	10-11	11-12	12-1	1-2	2-3	3-4	4-5	5-6	6-7	TOTAL
1	5.20	67.90	143.60	156.00	283.60	312.10	306.40	203.90	269.10	208.90	109.50	61.50	2.70	2210.4
2	13.50	71.80	95.50	114.60	195.40	77.90	31.40	69.40	151.70	64.00	*****	*****	*****	*****
3	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
4	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
5	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
6	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
7	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
8	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
9	13.20	72.90	146.40	214.30	263.00	300.90	300.70	269.30	240.20	14.80	2.90	3.70	1.50	*****
10	14.20	73.00	140.70	215.90	267.20	307.90	307.60	268.30	247.90	188.40	113.50	17.50	1.10	2175.2
11	14.60	71.00	90.70	193.20	62.00	219.20	308.30	112.10	76.90	156.50	90.70	14.70	1.60	2134.2
12	10.70	28.90	122.00	148.40	240.00	269.60	38.50	34.70	104.10	37.20	26.40	20.00	2.20	1234.6
13	20.20	69.40	152.30	210.50	261.20	297.00	302.90	265.60	244.20	101.20	59.70	26.50	2.20	1200.3
14	13.00	54.80	117.60	204.70	181.60	254.10	241.90	227.30	177.70	195.50	126.70	29.70	1.10	2202.3
15	15.70	78.10	134.20	209.10	177.00	300.20	304.30	294.20	248.00	95.70	34.00	21.60	2.00	1549.0
16	6.90	40.80	58.60	165.00	274.00	200.00	244.10	119.50	252.70	188.70	106.60	34.00	2.30	2093.1
17	14.10	09.90	157.60	207.00	196.30	61.60	165.30	245.80	237.60	66.50	93.40	47.60	3.70	1592.6
18	14.80	74.60	149.30	212.90	254.60	144.90	69.80	162.60	110.20	188.80	115.30	29.70	1.30	1690.3
19	6.50	47.40	152.90	127.30	230.30	272.00	116.80	244.50	81.00	103.10	99.10	53.10	2.10	1439.1
20	21.10	*****	*****	*****	*****	*****	*****	*****	*****	151.60	101.30	20.60	1.20	1533.4
21	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
22	13.00	59.10	119.10	185.10	281.70	283.10	224.60	47.00	204.90	74.20	54.90	47.60	2.00	*****
23	10.70	03.10	140.50	203.70	244.80	97.00	57.90	30.10	15.30	06.60	34.00	8.60	1.20	1548.0
24	3.10	27.40	53.40	177.40	265.60	203.70	44.50	124.90	102.60	11.50	9.70	7.60	1.00	892.9
25	7.70	58.40	130.00	193.70	223.90	198.80	122.00	228.00	64.30	55.10	34.20	16.10	2.00	1168.8
26	9.90	61.10	95.00	190.40	49.20	64.70	186.60	229.30	131.00	15.30	10.40	6.40	0.10	1276.2
27	3.70	20.50	75.00	192.50	251.30	256.90	267.20	238.60	205.40	73.40	70.40	12.60	*****	*****
28	6.90	69.10	135.70	170.00	221.20	260.50	295.50	275.70	197.60	01.60	41.00	19.00	*****	*****
29	14.00	60.90	129.90	206.20	239.10	268.50	304.80	185.60	88.30	44.70	25.30	12.70	*****	*****
30	13.00	71.70	127.70	193.00	262.10	203.20	253.60	54.50	213.70	76.20	57.20	22.70	*****	*****
MEAN	11.92	60.54	126.51	191.60	233.51	236.72	201.06	100.10	106.85	116.70	73.78	23.97	1.59	1626.9
STD D	15.29	15.80	31.39	23.74	55.01	75.37	145.07	100.00	84.57	65.74	39.57	14.57	0.69	211.7
MIN	3.10	27.40	53.40	127.30	62.00	61.60	36.50	30.10	15.30	11.50	9.70	7.60	0.10	447.6
MAX	26.20	78.10	157.60	215.90	283.60	312.10	306.70	294.20	269.10	206.90	126.70	61.50	3.70	2346.3

MONTHLY TOTAL SOLAR INSOLATION IN BTU/FT**2 /S. HOUR

MONTH: SEP 1978	3.00	6.00	9.00	12.00	15.00	18.00	21.00	24.00
0.00								
350.00								
341.03								
332.05								
323.08								
314.10								
305.13								
296.15								
287.18								
278.21								
269.23								
260.26								
251.28								
242.31								
233.33								
224.36								
215.38								
206.41								
197.44								
188.46								
179.49								
170.51								
161.54								
152.56								
143.59								
134.62								
125.64								
116.67								
107.69								
98.72								
89.74								
80.77								
71.79								
62.82								
53.85								
44.87								
35.90								
26.92								
17.95								
8.97								
0.00								

0.00
 3.00
 6.00
 9.00
 12.00
 15.00
 18.00
 21.00
 24.00

(+) MAXIMUM VALUE
 (M) MEAN VALUE
 (-) MINIMUM VALUE

FREQUENCY CHARTS FOR DISPERSE / TOTAL INSULATION

MONTH: SEP 1970

LOCATION: SACAROLI, CATAL.

BASED ON DAILY VALUES

REGULAR

RANGE	0	20	40	60	80	100	120	NO. OF VALUES	% OF TOTAL
0-.1								0	0.00
.1-.2	XXXXXXXXXXXXXXXXXXXX							56	11.17
.2-.3	XXXXXXXXXXXXXXXXXXXX							37	14.57
.3-.4	XXXXXXXXXXXXXXXXXXXX							53	12.99
.4-.5	XXXXXXXXXXXXXXXXXXXX							29	11.02
.5-.6	XXXXXXXXXXXX							23	9.16
.6-.7	XXXXXXXXXXXX							15	5.71
.7-.8	XXXXXXXXXXXX							15	6.30
.8-.9	XXXXXXXXXXXX							12	4.72
.9-1.	XXXXXXXXXXXX							14	5.51

THERE ARE 40 VALUES ABOVE 1.0 (15.75%)

CUMULATIVE

RANGE	0	80	160	240	320	400	480	NO. OF VALUES	% OF TOTAL
0-.1								0	0.00
.1-.2	XXXX							36	14.17
.2-.3	XXXXXXXXXXXX							73	28.74
.3-.4	XXXXXXXXXXXXXXXXXXXX							106	41.73
.4-.5	XXXXXXXXXXXXXXXXXXXX							154	52.76
.5-.6	XXXXXXXXXXXXXXXXXXXX							157	61.81
.6-.7	XXXXXXXXXXXXXXXXXXXX							172	74.02
.7-.8	XXXXXXXXXXXXXXXXXXXX							200	76.74
.8-.9	XXXXXXXXXXXXXXXXXXXX							214	84.25
.9-1.	XXXXXXXXXXXXXXXXXXXX								

BASED ON DAILY VALUES

CUMULATIVE

RANGE	0	5	10	15	20	25	30	NO. OF VALUES	% OF TOTAL
0-.1								0	0.00
.1-.2	XX							2	40.00
.2-.3	XX							0	40.00
.3-.4								1	20.00
.4-.5	X							0	0.00
.5-.6								0	0.00
.6-.7								0	0.00
.7-.8								0	0.00
.8-.9								0	0.00
.9-1.								0	0.00

MONTHLY PEATHEY DATA
 LOCATION: SACARAI, CATANDU
 TOTAL / EXTRATERRESTIAL INSOLATION

MONTH: SEP 1978

DAY	MONTHLY PEATHEY DATA												DAILY VALUE	
	6-7 (A)	7-8 (B)	8-9 (C)	9-10 (D)	10-11 (E)	11-12 (F)	12-1 (N)	1-2 (G)	2-3 (H)	3-4 (I)	4-5 (J)	5-6 (A)		6-7 (L)
1	0.450	0.527	0.643	0.514	0.779	0.777	0.743	0.715	0.758	0.719	0.528	0.553	0.155	0.682
2	0.450	0.557	0.441	0.378	0.536	0.194	0.076	0.175	0.425	0.221	0.528	0.553	0.155	0.682
3	0.450	0.557	0.441	0.378	0.536	0.194	0.076	0.175	0.425	0.221	0.528	0.553	0.155	0.682
4	0.450	0.557	0.441	0.378	0.536	0.194	0.076	0.175	0.425	0.221	0.528	0.553	0.155	0.682
5	0.450	0.557	0.441	0.378	0.536	0.194	0.076	0.175	0.425	0.221	0.528	0.553	0.155	0.682
6	0.450	0.557	0.441	0.378	0.536	0.194	0.076	0.175	0.425	0.221	0.528	0.553	0.155	0.682
7	0.450	0.557	0.441	0.378	0.536	0.194	0.076	0.175	0.425	0.221	0.528	0.553	0.155	0.682
8	0.450	0.557	0.441	0.378	0.536	0.194	0.076	0.175	0.425	0.221	0.528	0.553	0.155	0.682
9	0.444	0.564	0.655	0.706	0.723	0.753	0.754	0.739	0.708	0.652	0.015	0.037	0.131	0.682
10	0.479	0.572	0.665	0.711	0.735	0.753	0.753	0.738	0.715	0.670	0.577	0.178	0.103	0.682
11	0.494	0.550	0.406	0.636	0.171	0.549	0.755	0.282	0.228	0.559	0.496	0.152	0.162	0.682
12	0.363	0.224	0.546	0.555	0.661	0.676	0.094	0.089	0.302	0.133	0.137	0.218	0.240	0.390
13	0.891	0.538	0.681	0.720	0.720	0.746	0.744	0.735	0.710	0.364	0.311	0.283	0.260	0.382
14	0.443	0.425	0.526	0.694	0.501	0.639	0.595	0.568	0.314	0.707	0.665	0.322	0.141	0.694
15	0.538	0.606	0.601	0.690	0.490	0.755	0.750	0.761	0.726	0.340	0.180	0.382	0.279	0.495
16	0.237	0.317	0.263	0.611	0.757	0.504	0.603	0.309	0.742	0.684	0.568	0.382	0.351	0.660
17	0.487	0.544	0.707	0.684	0.543	0.155	0.409	0.638	0.700	0.244	0.502	0.545	0.620	0.504
18	0.513	0.581	0.670	0.704	0.705	0.366	0.173	0.423	0.349	0.696	0.624	0.347	0.240	0.540
19	0.226	0.370	0.687	0.421	0.636	0.688	0.269	0.638	0.240	0.382	0.541	0.394	0.430	0.465
20	0.739	0.463	0.536	0.615	0.783	0.398	0.701	0.734	0.413	0.491	0.558	0.250	0.273	0.495
21	0.461	0.495	0.634	0.677	0.681	0.247	0.561	0.124	0.614	0.279	0.307	0.600	0.573	0.682
22	0.381	0.216	0.241	0.590	0.740	0.672	0.145	0.079	0.046	0.044	0.192	0.111	0.369	0.504
23	0.111	0.460	0.615	0.646	0.625	0.508	0.112	0.330	0.309	0.213	0.055	0.100	0.370	0.292
24	0.278	0.483	0.430	0.635	0.130	0.658	0.308	0.604	0.195	0.059	0.196	0.216	0.341	0.385
25	0.360	0.162	0.340	0.643	0.704	0.165	0.470	0.609	0.398	0.302	0.109	0.115	0.050	0.420
26	0.136	0.549	0.617	0.569	0.620	0.692	0.674	0.636	0.626	0.316	0.411	0.179	0.050	0.420
27	0.523	0.485	0.591	0.691	0.620	0.692	0.747	0.737	0.605	0.174	0.241	0.272	0.050	0.420
28	0.329	0.573	0.502	0.648	0.672	0.742	0.772	0.498	0.271	0.174	0.150	0.186	0.050	0.420
29	0.430	0.472	0.568	0.634	0.738	0.738	0.644	0.147	1.659	0.604	0.457	0.144	0.050	0.420
30	0.412	0.472	0.568	0.634	0.646	0.602	0.496	0.466	0.489	0.426	0.394	0.268	0.297	0.520
31	0.180	0.123	0.141	0.076	0.153	0.189	0.257	0.256	0.245	0.236	0.206	0.141	0.164	0.120
32	0.111	0.210	0.241	0.421	0.171	0.155	0.094	0.079	0.046	0.044	0.055	0.100	0.050	0.292
33	0.891	0.606	0.707	0.711	0.783	0.777	0.755	0.761	0.758	0.719	0.665	0.555	0.642	0.694

MEAN
 STD 0
 MIN
 MAX

FREQUENCY CHARTS FOR TOTAL / EXTRATERRESTRIAL ISOLATION

MONTH: SEP 1976

LOCATION: SACARDI, CATANIA

BASED ON HOURLY VALUES

REGULAR

RANGE	0	20	40	60	80	100	120	NO. OF VALUES	% OF TOTAL
0-.1	XXXXXX							13	4.26
.1-.2	XXXXXXXXXXXXXXXXXX							36	11.61
.2-.3	XXXXXXXXXXXXXXXXXX							32	10.47
.3-.4	XXXXXXXXXXXXXXXXXX							36	11.60
.4-.5	XXXXXXXXXXXXXXXXXX							50	9.84
.5-.6	XXXXXXXXXXXXXXXXXX							44	14.43
.6-.7	XXXXXXXXXXXXXXXXXX							60	19.67
.7-.8	XXXXXXXXXXXXXXXXXX							53	17.58
.8-.9								1	0.33
.9-1.								0	0.00

CUMULATIVE

RANGE	0	80	160	240	320	400	480	NO. OF VALUES	% OF TOTAL
0-.1	X							13	4.26
.1-.2	XXXXXXXX							49	16.07
.2-.3	XXXXXXXXXX							61	20.56
.3-.4	XXXXXXXXXXXX							117	38.36
.4-.5	XXXXXXXXXXXXXX							147	48.20
.5-.6	XXXXXXXXXXXXXXXXXX							191	62.62
.6-.7	XXXXXXXXXXXXXXXXXXXX							251	82.30
.7-.8	XXXXXXXXXXXXXXXXXXXXXX							304	99.67
.8-.9	XXXXXXXXXXXXXXXXXXXXXXX							345	112.00
.9-1.	XXXXXXXXXXXXXXXXXXXXXXX							305	100.00

BASED ON DAILY VALUES

REGULAR

RANGE	0	5	10	15	NO. OF VALUES	% OF TOTAL	0	1K	2K	3K	NO. OF VALUES	% OF TOTAL
0-.1					0	0.00					0	0.00
.1-.2					0	0.00					0	0.00
.2-.3	X				1	5.00	X				1	5.00
.3-.4	XXX				3	17.65	XXX				4	23.53
.4-.5	XXXX				4	23.53	XXXXXX				8	47.06
.5-.6	XXXXX				4	23.53	XXXXXXXXXX				12	70.59
.6-.7	XXXXXX				5	29.41	XXXXXXXXXXXXXX				17	100.00
.7-.8					0	0.00	XXXXXXXXXXXXXXXXXX				17	100.00
.8-.9					0	0.00	XXXXXXXXXXXXXXXXXX				17	100.00
.9-1.					0	0.00	XXXXXXXXXXXXXXXXXX				17	100.00

CUMULATIVE

RANGE	0	5	10	15	NO. OF VALUES	% OF TOTAL	0	1K	2K	3K	NO. OF VALUES	% OF TOTAL
0-.1					0	0.00					0	0.00
.1-.2					0	0.00					0	0.00
.2-.3	X				1	5.00	X				1	5.00
.3-.4	XXX				3	17.65	XXX				4	23.53
.4-.5	XXXX				4	23.53	XXXXXX				8	47.06
.5-.6	XXXXX				4	23.53	XXXXXXXXXX				12	70.59
.6-.7	XXXXXX				5	29.41	XXXXXXXXXXXXXX				17	100.00
.7-.8					0	0.00	XXXXXXXXXXXXXXXXXX				17	100.00
.8-.9					0	0.00	XXXXXXXXXXXXXXXXXX				17	100.00
.9-1.					0	0.00	XXXXXXXXXXXXXXXXXX				17	100.00

MONTHLY WEATHER DATA

MONTH: SEP 1970

LOCATION: SACRAMENTO, CALIF.

DIFFUSE INSOLATION IN BTU/FT**2

DAY	HOUR												TOTAL	
	6-7	7-8	8-9	9-10	10-11	11-12	12-1	1-2	2-3	3-4	4-5	5-6		6-7
1	3.78	21.47	32.33	56.49	45.51	45.75	62.34	55.99	41.65	46.85	38.92	26.47	3.29	461.0
2	6.59	19.40	40.02	65.15	57.34	61.24	33.18	63.41	123.34	75.15	54.78	18.91	1.71	392.5
3	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
4	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
5	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
6	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
7	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
8	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
9	6.10	16.59	23.30	26.84	35.14	38.84	38.92	41.85	46.85	43.07	54.78	3.76	1.71	392.5
10	5.49	16.35	22.08	27.45	27.33	30.38	32.45	34.53	37.45	60.15	57.10	16.47	1.34	369.2
11	5.73	16.71	43.31	67.22	48.68	84.79	51.61	67.47	74.42	38.55	25.74	20.37	1.95	547.3
12	5.49	16.96	34.16	74.66	84.42	83.81	37.94	34.65	94.31	92.64	55.59	27.21	2.58	*****
13	*****	22.20	39.77	54.66	60.76	53.31	56.49	55.27	50.67	22.34	47.46	16.35	*****	*****
14	7.08	34.40	54.66	75.27	95.16	103.58	115.41	96.38	81.13	79.79	36.60	23.55	*****	*****
15	8.91	45.38	42.94	78.08	86.86	60.02	56.20	57.46	47.21	42.82	33.31	18.42	2.08	580.1
16	4.76	36.48	43.43	84.42	82.72	63.81	50.39	*****	50.14	51.61	52.22	32.33	*****	*****
17	5.73	15.98	47.46	60.88	58.44	61.12	82.47	52.34	43.31	30.74	23.79	12.32	*****	*****
18	6.95	22.20	35.26	55.14	66.12	60.02	58.44	63.94	74.79	67.71	44.65	25.86	*****	*****
19	4.76	31.84	72.71	74.54	119.32	113.46	101.14	88.57	63.81	62.46	79.30	23.91	*****	*****
20	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
21	9.27	32.70	44.53	62.22	72.59	154.33	166.48	132.25	86.21	80.40	58.68	40.75	*****	*****
22	6.59	24.52	36.55	49.29	63.20	58.68	85.52	53.56	119.93	84.06	*****	*****	*****	*****
23	2.32	22.08	47.09	62.46	50.24	61.24	62.95	55.87	*****	12.93	10.61	7.93	*****	*****
24	5.73	32.45	50.51	93.45	69.17	66.12	49.94	130.78	94.67	62.10	39.14	14.79	*****	*****
25	6.59	32.45	73.08	66.00	54.41	127.61	131.52	117.12	96.25	17.93	21.47	9.39	*****	*****
26	2.81	18.18	58.68	88.45	91.26	113.34	123.45	116.02	78.81	70.15	62.22	*****	*****	*****
27	9.52	36.97	31.72	63.32	67.95	56.97	112.36	83.08	122.85	69.42	*****	*****	*****	*****
28	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
29	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
30	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****

MEAN
STD D
MIN
MAX

6.00	23.30	32.79	51.22	48.70	47.46	49.56	46.29	41.97	20.15	2.39	470.0
1.85	12.53	10.23	23.26	22.95	14.41	14.40	8.29	13.61	3.81	0.76	51.2
3.78	16.35	22.08	26.84	27.33	30.38	32.45	36.55	25.74	16.47	1.34	313.3
8.91	45.38	43.31	78.08	86.86	84.79	62.34	60.15	57.10	26.47	3.29	698.6

MONTH: SEP 1975

MONTHLY WEATHER DATA

LOCATION: MACAPOI, LAHAINA

DIFFUSE / TOTAL I SOLAR IRR.

DAY	HOUR (CODE)												5-6 (K)	5-7 (L)	DAILY VALUE
	0-7 (A)	7-8 (B)	8-9 (C)	9-10 (D)	10-11 (E)	11-12 (F)	12-1 (G)	1-2 (G)	2-3 (H)	3-4 (I)	4-5 (J)	5-6 (K)			
1	0.727	0.316	0.225	0.362	0.160	0.147	0.203	0.127	0.156	0.224	0.355	0.434	1.220	0.209	
2	0.468	0.270	0.406	0.568	0.293	0.786	1.057	0.919	0.818	1.018	0.555	0.434	1.220	0.209	
3	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	
4	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	
5	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	
6	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	
7	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	
8	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	
9	0.462	0.228	0.159	0.125	0.134	0.129	0.126	0.145	0.190	1.113	0.968	1.022	1.139	0.209	
10	0.387	0.222	0.149	0.127	0.102	0.101	0.105	0.120	0.151	0.229	0.483	1.061	1.220	0.180	
11	0.393	0.235	0.478	0.348	0.785	0.367	0.167	0.013	0.943	0.354	0.590	1.120	1.220	0.175	
12	0.513	0.587	0.280	0.443	0.352	0.311	0.986	0.999	0.906	1.030	0.975	0.980	1.220	0.445	
13	*****	0.320	0.261	0.260	0.233	0.180	0.186	0.194	0.208	0.917	0.928	1.027	*****	*****	
14	0.544	0.628	0.465	0.368	0.524	0.408	0.477	0.437	0.753	0.260	0.375	0.554	*****	*****	
15	0.567	0.581	0.320	0.373	0.489	0.200	0.184	0.195	0.227	0.634	1.076	1.090	*****	*****	
16	0.690	0.894	0.741	0.456	0.302	0.319	0.206	0.213	0.198	0.824	0.312	0.542	1.107	0.277	
17	0.407	0.229	0.301	0.294	0.298	0.992	0.499	0.213	0.182	0.776	0.559	0.679	*****	*****	
18	0.470	0.298	0.236	0.259	0.260	0.414	0.837	0.516	0.675	0.163	0.206	0.415	*****	*****	
19	0.732	0.672	0.476	0.586	0.518	0.417	0.867	0.362	0.788	0.657	0.451	0.781	*****	*****	
20	*****	*****	*****	*****	*****	*****	*****	*****	*****	0.474	0.703	1.161	*****	*****	
21	0.713	0.553	0.374	0.336	0.258	0.983	0.598	0.472	0.637	0.084	1.069	0.056	*****	*****	
22	0.616	0.589	0.274	0.242	0.258	0.207	0.361	1.140	0.585	0.971	*****	1.177	*****	*****	
23	0.748	0.806	0.862	0.352	0.212	0.631	1.287	1.192	0.971	1.125	1.074	1.043	*****	*****	
24	0.745	0.556	0.371	0.482	0.309	0.251	1.121	1.047	0.971	1.127	1.145	1.167	*****	*****	
25	0.665	0.531	0.769	0.347	0.309	0.642	0.514	0.514	1.030	1.172	1.142	1.110	*****	*****	
26	0.758	0.887	0.782	0.459	1.106	1.250	0.664	0.520	0.602	0.895	0.884	*****	*****	*****	
27	1.069	0.535	0.234	0.372	0.363	0.441	0.421	0.348	0.598	0.851	*****	*****	*****	*****	
28	*****	*****	*****	*****	*****	0.211	*****	*****	*****	*****	*****	*****	*****	*****	
29	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	
30	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	

MEAN 0.507
 STD D 0.143
 MIN 0.387
 MAX 0.727

0.266
 0.137
 0.149
 0.478

0.334
 0.296
 0.102
 0.785

0.157
 0.041
 0.105
 0.203

0.193
 0.114
 0.101
 0.387

0.267
 0.129
 0.125
 0.373

0.420
 0.351
 0.224
 1.036

0.543
 0.265
 0.312
 0.975

0.631
 0.321
 0.430
 1.120

1.209
 0.024
 1.167
 1.220

0.240
 0.211
 0.120
 0.613

0.193
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 0.101
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0.267
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0.420
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